

**UNIVERSITY OF BOLTON**  
**SCHOOL OF ENGINEERING**  
**B.ENG (HONS) ELECTRICAL & ELECTRONIC**  
**ENGINEERING**  
**SEMESTER 1 EXAMINATION - 2024/2025**  
**ENGINEERING ELECTROMAGNETICS**  
**MODULE NO: EEE6012**

Date: Thursday 9<sup>th</sup> January 2025

Time: 2:00pm – 4:30pm

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**INSTRUCTIONS TO CANDIDATES:**

There are SIX questions.

Answer **ANY FOUR** questions.

All questions carry equal marks.

Marks for parts of questions are shown in brackets.

Electronic calculators may be used provided that data and program storage memory is cleared prior to the examination.

**CANDIDATES REQUIRE:**

Formula Sheet (attached).

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**Question 1**

- A. The waveform shown in red in figure Q1.A is given by  $v = 5 \cos\left(\frac{2\pi t}{8}\right)$ . There is a phase difference between the red and the other two waves. Write down the equation describing:

I. The green wave

**[4 marks]**

II. The blue wave

**[4 marks]**

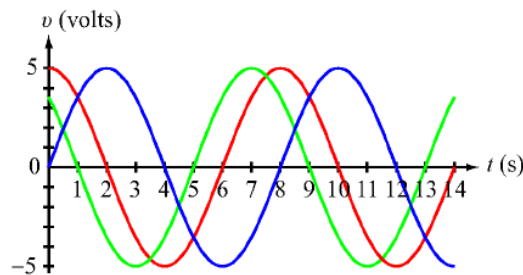


Figure Q1.A

- B. Transform vector  $\mathbf{A} = \hat{x}(x + y) + \hat{y}(y - x) + \hat{z}z$  from Cartesian to cylindrical coordinates.

**[8 marks]**

- C. A series RL circuit is connected to a voltage source given by  $v_s(t) = 150 \cos \omega t$  V. Find:

i. The phasor current

**[5 marks]**

ii. The instantaneous current  $i(t)$  for  $R = 400 \, \Omega$ ,  $L = 3 \, \text{mH}$  and  $\omega = 10^5 \, \text{rad/s}$ .

**[4 marks]**

**Total 25 marks**

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**Question 2**

- A. There are two points in Cartesian coordinates at  $P_1(1,2,3)$  and  $P_2(-1,-2,3)$ ,  
Find:
- I. The distance vector  $\overrightarrow{P_1P_2}$   
[3 marks]
  - II. The angle between vectors  $\overrightarrow{P_1}$  and  $\overrightarrow{P_2}$  using the cross product between them  
[3 marks]
  - III. The angle that vector  $\overrightarrow{P_2}$  makes with the z-axis  
[3 marks]
- B. Point  $P = (2\sqrt{3}, \frac{\pi}{3}, -2)$  is given in cylindrical coordinates. Express P in spherical coordinates.  
[6 marks]
- C. Given  $V = x^2y + xy^2 + xz^2$ , find:
- i. The gradient of V  
[5 marks]
  - ii. Evaluate the gradient at  $(1,-1,2)$   
[5 marks]

**Total 25 marks**

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**Question 3**

- A. A square plate in the x-y plane is situated in the space defined by  $-3m \leq x \leq 3m$  and  $-3m \leq y \leq 3m$ . Find the total charge on the plate if the surface charge density is given by  $\rho_s = 4y^2 \mu\text{C}/\text{m}^2$ . **[5 marks]**
- B. Four charges of  $10 \mu\text{C}$  each are located in free space at points with Cartesian coordinates  $(-3,0,0)$ ,  $(3,0,0)$ ,  $(0,-3,0)$  and  $(0,3,0)$ . Find the force on a  $20 \mu\text{C}$  charge located at  $(0,0,4)$ . All distances are in metres. **[10 marks]**
- C. A horizontal wire with a mass per unit length of  $0.2 \text{ kg/m}$  carries a current of  $4 \text{ A}$  in the  $+x$ -direction. If the wire is placed in a uniform magnetic flux density  $B$ , what should the direction and minimum magnitude of  $B$  to magnetically lift the wire vertically upward? The acceleration due to gravity is  $g = 9.8 \frac{\text{m}}{\text{s}^2}$ . **[6 marks]**
- D. A square coil of 100 turns and  $0.5 \text{ m}$ -long sides is in a region with a uniform magnetic flux density of  $0.2 \text{ Tesla}$ . If the maximum magnetic torque exerted on the coil is  $4 \times 10^{-2} \text{ N.m}$ , what is the current flowing in the coil? **[4 marks]**

**Total 25 marks**

**Question 4**

- A. A transmission line of length  $l$  connects a load to a sinusoidal voltage source with an oscillation frequency  $f$ . Assuming the velocity of wave propagation on the line is  $c$ , for which of the following situations it is reasonable to ignore the presence of the transmission line in the solution of the circuit and for which condition(s) it is nonnegligible to ignore.
- i.  $l = 20 \text{ cm}$ ,  $f = 20 \text{ kHz}$
  - ii.  $l = 50 \text{ cm}$ ,  $f = 60 \text{ Hz}$
  - iii.  $l = 20 \text{ cm}$ ,  $f = 600 \text{ MHz}$
  - iv.  $l = 1 \text{ mm}$ ,  $f = 100 \text{ GHz}$
- [5 marks]**
- B. A distortionless line has  $Z_0 = 60 \Omega$ ,  $\alpha = 20 \text{ Np/m}$ ,  $\mu = 0.6c$  where  $c$  is the speed of light in a vacuum, Find R, L, C and G at  $100 \text{ MHz}$ . **[20 marks]**

**Total 25 marks**

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**Question 5**

- A. The electric field phasor of a uniform plane wave is given by  $\tilde{E} = \hat{y}10e^{j0.2z}$  (V/m). If the phase velocity of the wave is  $1.5 \times 10^8$  m/s and the relative permeability of the medium is  $\mu_r = 2.4$ , find:
- Wavelength
  - Frequency
- [10 marks]**
- B. A plane wave in air with an electric field amplitude of 20 V/m is incident normally upon the surface of a lossless, nonmagnetic medium with  $\epsilon_r = 25$ . Determine the standing wave ratio in the air medium.
- [5 marks]**
- C. A 50-MHz plane wave with electric field amplitude of 50 V/m is normally incident in air onto a semi-infinite, perfect dielectric medium with  $\epsilon_r = 36$ . Determine (a)  $\Gamma$ , (b) the average power densities of the incident and reflected waves.
- [10 marks]**

**Total 25 marks**

**Question 6**

- A. A transponder with a bandwidth of 400 MHz uses polarization diversity. If the bandwidth allocated to transmit a single telephone channel is 4kHz, how many telephone channels can be carried by the transponder?
- [5 marks]**
- B. A remote sensing satellite is in circular orbit around the earth at an altitude of 1100 km above the earth's surface and the  $R_e = 6378$  km. What is its orbital period?
- [5 marks]**
- C. Calculate the equation 6a to 2.d.p for  $A = 8.2$  and  $T = 85.9$ .
- $$\int_{-\infty}^{\infty} A \operatorname{rect}(t)_T dt$$
- 6a
- [5 marks]**
- D. A geostationary satellite is at a distance of 40,000 km from a ground receiving station. The satellite transmitting antenna is a circular aperture with a 1-m diameter and the ground station uses a parabolic dish antenna with an effective diameter of 20 cm. If the satellite transmits 1 kW of power at 12 GHz and the ground receiver is characterized by a system noise temperature of 1,000 K, what would be the signal-to-noise ratio of a received TV signal with a bandwidth of 6 MHz? The antennas and the atmosphere may be assumed lossless.
- [10 marks]**

**Total 25 marks**

**END OF QUESTIONS**  
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### Formula sheet

These equations are given to save short-term memorisation of details of derived equations and are given without any explanation or definition of symbols; the student is expected to know the meanings and usage.

Time-domain sinusoidal functions  $z(t)$  and their cosine-reference phasor-domain counterparts  $\tilde{Z}$ , where  $z(t) = \Re [\tilde{Z}e^{j\omega t}]$ .

$z(t)$		$\tilde{Z}$
$A \cos \omega t$	$\longleftrightarrow$	$A$
$A \cos(\omega t + \phi_0)$	$\longleftrightarrow$	$Ae^{j\phi_0}$
$A \cos(\omega t + \beta x + \phi_0)$	$\longleftrightarrow$	$Ae^{j(\beta x + \phi_0)}$
$Ae^{-\alpha x} \cos(\omega t + \beta x + \phi_0)$	$\longleftrightarrow$	$Ae^{-\alpha x} e^{j(\beta x + \phi_0)}$
$A \sin \omega t$	$\longleftrightarrow$	$Ae^{-j\pi/2}$
$A \sin(\omega t + \phi_0)$	$\longleftrightarrow$	$Ae^{j(\phi_0 - \pi/2)}$
$\frac{d}{dt}(z(t))$	$\longleftrightarrow$	$j\omega \tilde{Z}$
$\frac{d}{dt}[A \cos(\omega t + \phi_0)]$	$\longleftrightarrow$	$j\omega Ae^{j\phi_0}$
$\int z(t) dt$	$\longleftrightarrow$	$\frac{1}{j\omega} \tilde{Z}$
$\int A \sin(\omega t + \phi_0) dt$	$\longleftrightarrow$	$\frac{1}{j\omega} Ae^{j(\phi_0 - \pi/2)}$

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Summary of vector relations.

	Cartesian Coordinates	Cylindrical Coordinates	Spherical Coordinates
<b>Coordinate variables</b>	$x, y, z$	$r, \phi, z$	$R, \theta, \phi$
<b>Vector representation</b> $\mathbf{A} =$	$\hat{x}A_x + \hat{y}A_y + \hat{z}A_z$	$\hat{r}A_r + \hat{\phi}A_\phi + \hat{z}A_z$	$\hat{R}A_R + \hat{\theta}A_\theta + \hat{\phi}A_\phi$
<b>Magnitude of A</b> $ \mathbf{A}  =$	$\sqrt{A_x^2 + A_y^2 + A_z^2}$	$\sqrt{A_r^2 + A_\phi^2 + A_z^2}$	$\sqrt{A_R^2 + A_\theta^2 + A_\phi^2}$
<b>Position vector</b> $\overrightarrow{OP_1} =$	$\hat{x}x_1 + \hat{y}y_1 + \hat{z}z_1,$ for $P = (x_1, y_1, z_1)$	$\hat{r}r_1 + \hat{z}z_1,$ for $P = (r_1, \phi_1, z_1)$	$\hat{R}R_1,$ for $P = (R_1, \theta_1, \phi_1)$
<b>Base vectors properties</b>	$\hat{x} \cdot \hat{x} = \hat{y} \cdot \hat{y} = \hat{z} \cdot \hat{z} = 1$ $\hat{x} \cdot \hat{y} = \hat{y} \cdot \hat{z} = \hat{z} \cdot \hat{x} = 0$ $\hat{x} \times \hat{y} = \hat{z}$ $\hat{y} \times \hat{z} = \hat{x}$ $\hat{z} \times \hat{x} = \hat{y}$	$\hat{r} \cdot \hat{r} = \hat{\phi} \cdot \hat{\phi} = \hat{z} \cdot \hat{z} = 1$ $\hat{r} \cdot \hat{\phi} = \hat{\phi} \cdot \hat{z} = \hat{z} \cdot \hat{r} = 0$ $\hat{r} \times \hat{\phi} = \hat{z}$ $\hat{\phi} \times \hat{z} = \hat{r}$ $\hat{z} \times \hat{r} = \hat{\phi}$	$\hat{R} \cdot \hat{R} = \hat{\theta} \cdot \hat{\theta} = \hat{\phi} \cdot \hat{\phi} = 1$ $\hat{R} \cdot \hat{\theta} = \hat{\theta} \cdot \hat{\phi} = \hat{\phi} \cdot \hat{R} = 0$ $\hat{R} \times \hat{\theta} = \hat{\phi}$ $\hat{\theta} \times \hat{\phi} = \hat{R}$ $\hat{\phi} \times \hat{R} = \hat{\theta}$
<b>Dot product</b> $\mathbf{A} \cdot \mathbf{B} =$	$A_x B_x + A_y B_y + A_z B_z$	$A_r B_r + A_\phi B_\phi + A_z B_z$	$A_R B_R + A_\theta B_\theta + A_\phi B_\phi$
<b>Cross product</b> $\mathbf{A} \times \mathbf{B} =$	$\begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{r} & \hat{\phi} & \hat{z} \\ A_r & A_\phi & A_z \\ B_r & B_\phi & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{R} & \hat{\theta} & \hat{\phi} \\ A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \end{vmatrix}$
<b>Differential length</b> $d\mathbf{l} =$	$\hat{x} dx + \hat{y} dy + \hat{z} dz$	$\hat{r} dr + \hat{\phi} r d\phi + \hat{z} dz$	$\hat{R} dR + \hat{\theta} R d\theta + \hat{\phi} R \sin \theta d\phi$
<b>Differential surface areas</b>	$ds_x = \hat{x} dy dz$ $ds_y = \hat{y} dx dz$ $ds_z = \hat{z} dx dy$	$ds_r = \hat{r} r d\phi dz$ $ds_\phi = \hat{\phi} dr dz$ $ds_z = \hat{z} r dr d\phi$	$ds_R = \hat{R} R^2 \sin \theta d\theta d\phi$ $ds_\theta = \hat{\theta} R \sin \theta dR d\phi$ $ds_\phi = \hat{\phi} R dR d\theta$
<b>Differential volume</b> $dV =$	$dx dy dz$	$r dr d\phi dz$	$R^2 \sin \theta dR d\theta d\phi$

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Coordinate transformation relations.

Transformation	Coordinate Variables	Unit Vectors	Vector Components
<b>Cartesian to cylindrical</b>	$r = \sqrt{x^2 + y^2}$ $\phi = \tan^{-1}(y/x)$ $z = z$	$\hat{r} = \hat{x} \cos \phi + \hat{y} \sin \phi$ $\hat{\phi} = -\hat{x} \sin \phi + \hat{y} \cos \phi$ $\hat{z} = \hat{z}$	$A_r = A_x \cos \phi + A_y \sin \phi$ $A_\phi = -A_x \sin \phi + A_y \cos \phi$ $A_z = A_z$
<b>Cylindrical to Cartesian</b>	$x = r \cos \phi$ $y = r \sin \phi$ $z = z$	$\hat{x} = \hat{r} \cos \phi - \hat{\phi} \sin \phi$ $\hat{y} = \hat{r} \sin \phi + \hat{\phi} \cos \phi$ $\hat{z} = \hat{z}$	$A_x = A_r \cos \phi - A_\phi \sin \phi$ $A_y = A_r \sin \phi + A_\phi \cos \phi$ $A_z = A_z$
<b>Cartesian to spherical</b>	$R = \sqrt{x^2 + y^2 + z^2}$ $\theta = \tan^{-1}[\sqrt{x^2 + y^2}/z]$ $\phi = \tan^{-1}(y/x)$	$\hat{R} = \hat{x} \sin \theta \cos \phi + \hat{y} \sin \theta \sin \phi + \hat{z} \cos \theta$ $\hat{\theta} = \hat{x} \cos \theta \cos \phi + \hat{y} \cos \theta \sin \phi - \hat{z} \sin \theta$ $\hat{\phi} = -\hat{x} \sin \phi + \hat{y} \cos \phi$	$A_R = A_x \sin \theta \cos \phi + A_y \sin \theta \sin \phi + A_z \cos \theta$ $A_\theta = A_x \cos \theta \cos \phi + A_y \cos \theta \sin \phi - A_z \sin \theta$ $A_\phi = -A_x \sin \phi + A_y \cos \phi$
<b>Spherical to Cartesian</b>	$x = R \sin \theta \cos \phi$ $y = R \sin \theta \sin \phi$ $z = R \cos \theta$	$\hat{x} = \hat{R} \sin \theta \cos \phi + \hat{\theta} \cos \theta \cos \phi - \hat{\phi} \sin \phi$ $\hat{y} = \hat{R} \sin \theta \sin \phi + \hat{\theta} \cos \theta \sin \phi + \hat{\phi} \cos \phi$ $\hat{z} = \hat{R} \cos \theta - \hat{\theta} \sin \theta$	$A_x = A_R \sin \theta \cos \phi + A_\theta \cos \theta \cos \phi - A_\phi \sin \phi$ $A_y = A_R \sin \theta \sin \phi + A_\theta \cos \theta \sin \phi + A_\phi \cos \phi$ $A_z = A_R \cos \theta - A_\theta \sin \theta$
<b>Cylindrical to spherical</b>	$R = \sqrt{r^2 + z^2}$ $\theta = \tan^{-1}(r/z)$ $\phi = \phi$	$\hat{R} = \hat{r} \sin \theta + \hat{z} \cos \theta$ $\hat{\theta} = \hat{r} \cos \theta - \hat{z} \sin \theta$ $\hat{\phi} = \hat{\phi}$	$A_R = A_r \sin \theta + A_z \cos \theta$ $A_\theta = A_r \cos \theta - A_z \sin \theta$ $A_\phi = A_\phi$
<b>Spherical to cylindrical</b>	$r = R \sin \theta$ $\phi = \phi$ $z = R \cos \theta$	$\hat{r} = \hat{R} \sin \theta + \hat{\theta} \cos \theta$ $\hat{\phi} = \hat{\phi}$ $\hat{z} = \hat{R} \cos \theta - \hat{\theta} \sin \theta$	$A_r = A_R \sin \theta + A_\theta \cos \theta$ $A_\phi = A_\phi$ $A_z = A_R \cos \theta - A_\theta \sin \theta$

**ELECTROSTATICS:**

$$\begin{aligned}
 \mathbf{F}_{12} &= \frac{Q_1 Q_2}{4\pi\epsilon_0 R^2} \mathbf{a}_{R_{12}}, \quad \mathbf{F} = \frac{Q}{4\pi\epsilon_0} \sum_{k=1}^N \frac{Q_k (\mathbf{r} - \mathbf{r}_k)}{|\mathbf{r} - \mathbf{r}_k|^3}, \quad \mathbf{E} = \frac{\mathbf{F}}{Q}, \quad \mathbf{E} = \int \frac{\rho_L dl}{4\pi\epsilon_0 R^2} \mathbf{a}_R, \quad \mathbf{E} = \int \frac{\rho_S dS}{4\pi\epsilon_0 R^2} \mathbf{a}_R, \quad \mathbf{E} = \int \frac{\rho_v dv}{4\pi\epsilon_0 R^2} \mathbf{a}_R \\
 \mathbf{E} &= \frac{\rho_S}{2\epsilon_0} \mathbf{a}_n, \quad \mathbf{E} = \frac{\rho_L}{2\pi\epsilon_0 \rho} \mathbf{a}_\rho, \quad Q = \oint_S \mathbf{D} \cdot d\mathbf{S} = \int_V \rho_v dv, \quad \nabla \cdot \mathbf{D} = \rho_v, \quad W = -Q \int_A^B \mathbf{E} \cdot d\ell, \quad V_{AB} = \frac{W}{Q} = -\int_A^B \mathbf{E} \cdot d\ell, \quad V = \frac{Q}{4\pi\epsilon_0 r} \\
 \oint \mathbf{E} \cdot d\ell &= 0, \quad \nabla \times \mathbf{E} = 0, \quad \mathbf{E} = -\nabla V, \quad W_E = \frac{1}{2} \sum_{k=1}^n Q_k V_k, \quad W_E = \frac{1}{2} \int \mathbf{D} \cdot \mathbf{E} dv = \frac{1}{2} \int \epsilon_0 E^2 dv, \quad \mathbf{J} = \rho_v \mathbf{u}, \quad I = \int_S \mathbf{J} \cdot d\mathbf{S}, \quad \mathbf{J} = \sigma \mathbf{E}, \\
 R &= \frac{V}{I} = \frac{\int \mathbf{E} \cdot d\mathbf{l}}{\int \sigma \mathbf{E} \cdot d\mathbf{S}}, \quad \mathbf{D} = \epsilon \mathbf{E}, \quad \nabla \cdot \mathbf{J} = -\frac{\partial \rho_v}{\partial t}, \quad E_{1t} = E_{2t}, \quad D_{1n} - D_{2n} = \rho_s, \quad D_{1n} = D_{2n}, \quad \frac{\tan \theta_1}{\tan \theta_2} = \frac{\epsilon_{r1}}{\epsilon_{r2}} \\
 \nabla^2 V &= -\frac{\rho_v}{\epsilon}, \quad \nabla^2 V = 0, \quad C = \frac{Q}{V} = \frac{\epsilon \oint \mathbf{E} \cdot d\mathbf{S}}{\int \mathbf{E} \cdot d\mathbf{l}}, \quad W_E = \frac{1}{2} CV^2 = \frac{1}{2} QV = \frac{Q^2}{2C}, \quad C = \frac{Q}{V} = \frac{2\pi\epsilon L}{\ln \frac{b}{a}}, \quad C = \frac{Q}{V} = \frac{4\pi\epsilon}{\frac{1}{a} - \frac{1}{b}}, \quad RC = \frac{\epsilon}{\sigma}
 \end{aligned}$$

$$\epsilon_0 = 8.85 \times 10^{-12} \text{ F/m}, \quad \mu_0 = 4\pi \times 10^{-7} \text{ H/m}$$

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**MAGNETOSTATICS:**

$$\mathbf{H} = \int_L \frac{Id\mathbf{l} \times \mathbf{a}_R}{4\pi R^2}, \quad \mathbf{H} = \int_S \frac{\mathbf{K}dS \times \mathbf{a}_R}{4\pi R^2}, \quad \mathbf{H} = \int_V \frac{\mathbf{J}dv \times \mathbf{a}_R}{4\pi R^2}, \quad \mathbf{H} = \frac{I}{4\pi\rho}(\cos\alpha_2 - \cos\alpha_1)\mathbf{a}_\phi, \quad \mathbf{H} = \frac{I}{2\pi\rho}\mathbf{a}_\phi, \quad \mathbf{a}_\phi = \mathbf{a}_\ell \times \mathbf{a}_\rho,$$

$$\oint \mathbf{H} \cdot d\mathbf{l} = I_{enc}, \quad \nabla \times \mathbf{H} = \mathbf{J}, \quad \mathbf{H} = \frac{I}{2\pi\rho}\mathbf{a}_\phi, \quad \mathbf{H} = \frac{1}{2}\mathbf{K} \times \mathbf{a}_n, \quad \mathbf{B} = \mu\mathbf{H}, \quad \Psi = \int_S \mathbf{B} \cdot d\mathbf{S}, \quad \oint \mathbf{B} \cdot d\mathbf{S} = 0, \quad \nabla \cdot \mathbf{B} = 0, \quad \mathbf{H} = -\nabla V_m,$$

$$\mathbf{B} = \nabla \times \mathbf{A}, \quad \mathbf{A} = \int_L \frac{\mu_0 Id\mathbf{l}}{4\pi R}, \quad \mathbf{A} = \int_S \frac{\mu_0 \mathbf{K}dS}{4\pi R}, \quad \mathbf{A} = \int_V \frac{\mu_0 \mathbf{J}dv}{4\pi R}, \quad \Psi = \oint_L \mathbf{A} \cdot d\mathbf{l}, \quad \mathbf{F} = Q(\mathbf{E} + \mathbf{u} \times \mathbf{B}), \quad d\mathbf{F} = Id\mathbf{l} \times \mathbf{B}, \quad \mathbf{B}_{1n} = \mathbf{B}_{2n},$$

$$(\mathbf{H}_1 - \mathbf{H}_2) \times \mathbf{a}_{n12} = \mathbf{K}, \quad \mathbf{H}_{1t} = \mathbf{H}_{2t}, \quad \frac{\tan\theta_1}{\tan\theta_2} = \frac{\mu_1}{\mu_2}, \quad L = \frac{\lambda}{I} = \frac{N\psi}{I}, \quad M_{12} = \frac{\lambda_{12}}{I_2} = \frac{N_1\psi_{12}}{I_2}, \quad W_m = \frac{1}{2} \int \mathbf{B} \cdot \mathbf{H}dv = \frac{1}{2} \int \mu H^2 dv$$

**WAVES AND APPLICATIONS:**

$$V_{emf} = -\frac{d\psi}{dt}, \quad V_{emf} = \oint_L \mathbf{E} \cdot d\mathbf{l} = -\int_S \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S}, \quad \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}, \quad V_{emf} = \oint_L \mathbf{E}_m \cdot d\mathbf{l} = \oint_L (\mathbf{u} \times \mathbf{B}) \cdot d\mathbf{l}$$

$$V_{emf} = \oint_L \mathbf{E} \cdot d\mathbf{l} = -\int_S \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S} + \oint_L (\mathbf{u} \times \mathbf{B}) \cdot d\mathbf{l}, \quad \mathbf{J}_d = \frac{\partial \mathbf{D}}{\partial t}, \quad \nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}, \quad \beta = \frac{2\pi}{\lambda}, \quad \underline{\gamma} = \alpha + j\beta$$

$$\alpha = \omega \sqrt{\frac{\mu\epsilon}{2} \left[ \sqrt{1 + \left[ \frac{\sigma}{\omega\epsilon} \right]^2} - 1 \right]}, \quad \beta = \omega \sqrt{\frac{\mu\epsilon}{2} \left[ \sqrt{1 + \left[ \frac{\sigma}{\omega\epsilon} \right]^2} + 1 \right]}, \quad \mathbf{E}(z, t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \mathbf{a}_x$$

$$|\underline{\eta}| = \frac{\sqrt{\mu/\epsilon}}{\left[ 1 + \left( \frac{\sigma}{\omega\epsilon} \right)^2 \right]^{1/4}}, \quad \tan 2\theta_\eta = \frac{\sigma}{\omega\epsilon}, \quad \mathbf{H} = \frac{E_0}{|\underline{\eta}|} e^{-\alpha z} \cos(\omega t - \beta z - \theta_\eta) \mathbf{a}_y, \quad \tan \theta = \frac{\sigma}{\omega\epsilon}, \quad \mathbf{a}_E \times \mathbf{a}_H = \mathbf{a}_k$$

$$\eta_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi \approx 377\Omega, \quad p(t) = \mathbf{E} \times \mathbf{H}, \quad p_{ave}(z) = \frac{1}{2} \text{Re}(\mathbf{E}_s \times \mathbf{H}_s^*), \quad p_{ave}(z) = \frac{E_0^2}{2|\underline{\eta}|} e^{-2\alpha z} \cos\theta_\eta \mathbf{a}_z, \quad P_{ave} = \int_S p_{ave} \cdot d\mathbf{S},$$

$$\Gamma = \frac{E_{ro}}{E_{io}} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}, \quad \tau = \frac{E_{to}}{E_{io}} = \frac{2\eta_2}{\eta_2 + \eta_1}, \quad s = \frac{|\mathbf{E}_1|_{\max}}{|\mathbf{E}_1|_{\min}} = \frac{|\mathbf{H}_1|_{\max}}{|\mathbf{H}_1|_{\min}} = \frac{1 + |\Gamma|}{1 - |\Gamma|}, \quad k_i \sin\theta_i = k_t \sin\theta_t,$$

$$\Gamma_{\parallel} = \frac{E_{ro}}{E_{io}} = \frac{\eta_2 \cos\theta_t - \eta_1 \cos\theta_i}{\eta_2 \cos\theta_t + \eta_1 \cos\theta_i}, \quad \tau_{\parallel} = \frac{E_{to}}{E_{io}} = \frac{2\eta_2 \cos\theta_i}{\eta_2 \cos\theta_t + \eta_1 \cos\theta_i}, \quad \sin^2 \theta_{B\parallel} = \frac{1 - \mu_2 \epsilon_1 / \mu_1 \epsilon_2}{1 - (\epsilon_1 / \epsilon_2)^2},$$

$$\Gamma_{\perp} = \frac{E_{ro}}{E_{io}} = \frac{\eta_2 \cos\theta_i - \eta_1 \cos\theta_t}{\eta_2 \cos\theta_i + \eta_1 \cos\theta_t}, \quad \tau_{\perp} = \frac{E_{to}}{E_{io}} = \frac{2\eta_2 \cos\theta_i}{\eta_2 \cos\theta_i + \eta_1 \cos\theta_t}, \quad \sin^2 \theta_{B\perp} = \frac{1 - \mu_1 \epsilon_2 / \mu_2 \epsilon_1}{1 - (\mu_1 / \mu_2)^2}$$

$$\omega = \beta c$$

$$S = \frac{|V_{max}|}{|V_{min}|} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

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ENGINEERING ELECTROMAGNETISM  
MODULE NO. EEE6012

## Antenna and Radar formula

### Dipole

Solid angle:

$$\Omega_p = \iint_{4\pi} F(\theta, \phi) d\Omega$$

Directivity:

Shorted dipole

Hertzian  
monopole

$$D = \frac{4\pi}{\Omega_p} \quad \text{or} \quad D = \frac{4\pi A_e}{\lambda^2}$$

$$S_0 = \frac{15\pi I_0^2}{R^2} \left( \frac{l}{\lambda} \right)^2$$

$$R_{\text{rad}} = 80\pi^2 \left[ \frac{dl}{\lambda} \right]^2$$

$$P_{\text{rad}} = \frac{1}{2} I_0^2 R_{\text{rad}}$$

$$R_{\text{rad}} = 80\pi^2 \left( \frac{l}{\lambda} \right)^2$$

### Half –wave dipole

$$\tilde{E}_\theta = j 60 I_0 \left\{ \frac{\cos[(\pi/2) \cos \theta]}{\sin \theta} \right\} \left( \frac{e^{-jkR}}{R} \right),$$

$$\tilde{H}_\phi = \frac{\tilde{E}_\theta}{\eta_0}.$$

$$|E_{\phi s}| = \frac{\eta_0 I_0 \cos \left( \frac{\pi}{2} \cos \theta \right)}{2\pi r \sin \theta}$$

$$|H_{\phi s}| = \frac{I_0 \cos \left( \frac{\pi}{2} \cos \theta \right)}{2\pi r \sin \theta}$$

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For Transmission line

	Propagation Constant $\gamma = \alpha + j\beta$	Phase Velocity $u_p$	Characteristic Impedance $Z_0$
<b>General case</b>	$\gamma = \sqrt{(R' + j\omega L')(G' + j\omega C')}$	$u_p = \omega/\beta$	$Z_0 = \sqrt{\frac{(R' + j\omega L')}{(G' + j\omega C')}}$
<b>Lossless</b> ( $R' = G' = 0$ )	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = \sqrt{L'/C'}$
<b>Lossless coaxial</b>	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = (60/\sqrt{\epsilon_r}) \ln(b/a)$
<b>Lossless two-wire</b>	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = \frac{(120/\sqrt{\epsilon_r})}{\ln[(D/d) + \sqrt{(D/d)^2 - 1}]}$ $Z_0 \simeq (120/\sqrt{\epsilon_r}) \ln(2D/d),$ if $D \gg d$
<b>Lossless parallel-plate</b>	$\alpha = 0, \beta = \omega\sqrt{\epsilon_r}/c$	$u_p = c/\sqrt{\epsilon_r}$	$Z_0 = (120\pi/\sqrt{\epsilon_r}) (h/w)$

Notes: (1)  $\mu = \mu_0$ ,  $\epsilon = \epsilon_r \epsilon_0$ ,  $c = 1/\sqrt{\mu_0 \epsilon_0}$ , and  $\sqrt{\mu_0/\epsilon_0} \simeq (120\pi) \Omega$ , where  $\epsilon_r$  is the relative permittivity of insulating material. (2) For coaxial line,  $a$  and  $b$  are radii of inner and outer conductors. (3) For two-wire line,  $d$  = wire diameter and  $D$  = separation between wire centers. (4) For parallel-plate line,  $w$  = width of plate and  $h$  = separation between the plates.

Distortionless line

$$\gamma = \sqrt{RG} + j\omega\sqrt{LC}$$

$$\frac{R}{L} = \frac{G}{C}, \quad Z_0 = \sqrt{\frac{L}{C}}$$

Open-circuited line

$$\tilde{V}_{oc}(d) = V_0^+ [e^{j\beta d} + e^{-j\beta d}] = 2V_0^+ \cos \beta d,$$

$$\tilde{I}_{oc}(d) = \frac{V_0^+}{Z_0} [e^{j\beta d} - e^{-j\beta d}] = \frac{2jV_0^+}{Z_0} \sin \beta d,$$

$$Z_{in}^{oc} = \frac{\tilde{V}_{oc}(l)}{\tilde{I}_{oc}(l)} = -jZ_0 \cot \beta l.$$

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### Short-circuited line

$$\tilde{V}_{sc}(d) = V_0^+[e^{j\beta d} - e^{-j\beta d}] = 2jV_0^+ \sin \beta d,$$

$$\tilde{I}_{sc}(d) = \frac{V_0^+}{Z_0}[e^{j\beta d} + e^{-j\beta d}] = \frac{2V_0^+}{Z_0} \cos \beta d,$$

$$Z_{sc}(d) = \frac{\tilde{V}_{sc}(d)}{\tilde{I}_{sc}(d)} = jZ_0 \tan \beta d.$$

$$j\omega L_{eq} = jZ_0 \tan \beta l, \quad \text{if } \tan \beta l \geq 0$$

$$\frac{1}{j\omega C_{eq}} = jZ_0 \tan \beta l, \quad \text{if } \tan \beta l \leq 0$$

$$Z_{in} = Z_0 \left[ \frac{Z_L + jZ_0 \tan \beta \ell}{Z_0 + jZ_L \tan \beta \ell} \right]$$

$$Z_{in} = Z_0 \left[ \frac{Z_L + Z_0 \tanh \gamma \ell}{Z_0 + Z_L \tanh \gamma \ell} \right]$$

$$V_o = \frac{Z_{in}}{Z_{in} + Z_g} V_g, \quad I_o = \frac{V_g}{Z_{in} + Z_g}$$

$$V_o = V_L e^{j\beta \ell}$$

For a bistatic radar (one in which the transmitting and receiving antennas are separated), the power received is given by

$$P_r = \frac{G_{dt}G_{dr}}{4\pi} \left[ \frac{\lambda}{4\pi r_1 r_2} \right]^2 \sigma P_{rad}$$

For a monostatic radar,  $r_1 = r_2 = r$  and  $G_{dt} = G_{dr}$ .

$$P_{rec} = P_t G_t G_r \left( \frac{\lambda}{4\pi R} \right)^2$$

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