# UNIVERSITY OF BOLTON SCHOOL OF ENGINEERING BEng (Hons) MECHANICAL ENGINEERING SEMESTER ONE EXAMINATION 2024/25 ADVANCED THEMOFLUID & CONTROL SYSTEMS MODULE NO: AME6015

Date: Friday 10<sup>th</sup> January 2025 Time: 10:00 – 12:00

<u>INSTRUCTIONS TO CANDIDATES:</u> There are <u>SIX</u> questions.

Answer ANY FOUR questions.

All questions carry equal marks.

Marks for parts of questions are shown

in brackets.

This examination paper carries a total of

100 marks.

All working must be shown. A numerical solution to a question obtained by programming an electronic

calculator will not be accepted.

### **QUESTION 1**

The landing craft suspension System and free body diagram at a landing operation is shown in Figure Q1.

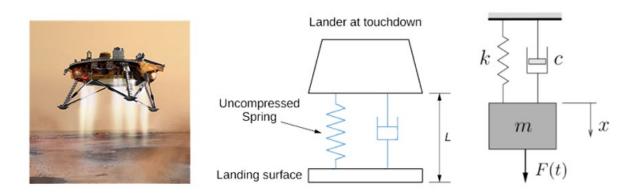


Figure Q1 The landing craft suspension System

(a) Derive the differential equations describing the behaviour of the system in Figure Q1 giving the relationship between the input force and the output of displacement x.

[6 Marks]

(b) Write out the transfer function expression for this system using Laplace transform if m =5kg, c = 35Ns/m, k=350N/m, force F(t) = 300F(t) and assuming zero initial condition.

[7 Marks]

(c) State the number of poles and zeros in the system. Give reasons for your answer.

[4 Marks]

(d) Check for if the system is controllable and observable.

[8 Marks]

**Total 25 marks** 

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### **QUESTION 2**

A PID controller is used to control a servo control system as shown in **Figure Q2**. The open loop transfer function of the plant is given by

$$G_p(s) = \frac{60}{(s+2)(s+5)}$$

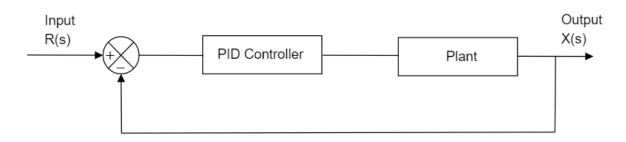


Figure Q2: Control system of the processing plant.

a) Evaluate the performances of closed loop servo control system (natural frequency, damping ratio, Percentage Overshoot, peak time, rise time, settling time and steady-state error) to assess its performance without the PID controller.

(10marks)

- b) Design a PD controller to determine the parameter  $K_p$  and  $K_d$ , and clearly identify the design procedure if the system responses for a unit step input are required as:
  - The maximum overshoot is less than 8%.
  - The settling time is 55% less than that of without the PD controller.

(15 marks)

**Total 25 marks** 

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### **QUESTION 3**

Why is it necessary to use a Digital-to-Analog Converter in a control system with digital controllers and analog actuators? [5 Marks]

b) If a Pneumatic control system as shown in Figure Q3 (a) shows the system consists of a Digital to Analogue Converter with a zero-order hold element in series with the Pneumatic control which has a transfer function;

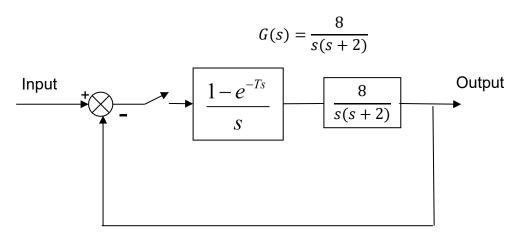


Figure Q3 (a) A Pneumatic control system

I. Find the sampled-data transfer function, G(z) for the digital control system. The sampling time, T, is 0.45 seconds.[8 Marks]

II. What is the resolution of the AD converter? [3 Marks]

III. What integer number represented a value of 8 Volts? [3 Marks]

IV. What voltage does the integer 150 represent? [3 Marks]

V. What voltage does 10101101 represent? [3 Marks]

**Total 25 marks** 

### **QUESTION 4**

A horizontal pipe with an internal diameter of 0.02 meters and a length of 10 metres carries water at a steady velocity of 0.01 m/s as shown in **Figure 4**. The water has a density ( $\rho$ ) of 1000 kg/m³ and a dynamic viscosity ( $\mu$ ) of 0.001 kg/m-s. A Computational Fluid Dynamics (CFD) simulation predicts a pressure difference of 7.73 Pa between the inlet and outlet of the pipe.

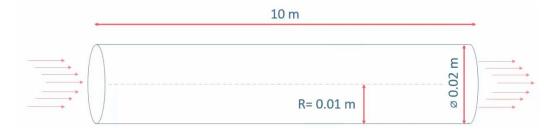


Figure 4 Flow through Pipe

a. Based on the given data calculate the Reynolds number for the flow and determine whether the flow is laminar or turbulent.

[3 Marks]

b. Select the appropriate formula for calculating the friction factor for the flow and determine the head loss in metres.

[7 Marks]

c. Calculate the pressure difference analytically and compare this analytical pressure difference with the CFD result. Moreover, calculate the percentage error between the analytical and CFD pressure differences.

[10 Marks]

d. Explain the three main steps involved in a typical Computational Fluid Dynamics (CFD) simulation.

[5 Marks]

Total 25 marks PLEASE TURN THE PAGE

### **QUESTION 5**

A military jet, designed for supersonic speeds, is cruising at Mach 2 (approximately 680 m/s) at an altitude where the air density is 0.2 kg/m³. The jet is powered by two turbojet engines, each with an air intake of 50 kg/s and an exhaust velocity of 1,200 m/s relative to the jet. This supersonic jet's propulsion relies on the principles of thrust generated by accelerating a mass of air backward. For the purposes of this calculation, assume steady-level flight with no significant altitude changes. Your task is to provide the following information based on the given scenario:



a) Calculate the thrust produced by one engine.

[5 Marks]

b) Determine the total thrust produced by both engines.

[4 Marks]

c) Estimate the fuel consumption if each engine has a specific fuel consumption (SFC) of 0.8 kg/(N·hr).

[8 Marks]

d) What are the basic principles of jet propulsion, and how does Newton's Third Law of Motion apply to it?

[8 Marks]

Total 25 marks PLEASE TURN THE PAGE

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**QUESTION 6** 

A jet aircraft is powered by a turbojet engine that needs to produce a thrust of 30,000 N to maintain a cruising speed of 250 m/s. The engine operates by accelerating the incoming air to an exhaust velocity of 800 m/s relative to the jet. Your task is to provide the following information based on the given scenario:

a) Calculate the mass flow rate of air required to achieve this thrust.

[10 Marks]

b) Calculate the propulsive efficiency of the engine.

[10 Marks]

c) If jet engine has a propulsive power of 6 MW and a total energy input rate of 15 MW (based on fuel combustion). Calculate the thermal efficiency of the engine
 [5 Marks]

**Total 25 marks** 

**END OF QUESTIONS** 

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## Formula Sheet

# Blocks with feedback loop

$$G(s) = \frac{Go(s)}{1 + Go(s)H(s)}$$
 (for a negative feedback)

G(s) = 
$$\frac{Go(s)}{1 - Go(s)H(s)}$$
 (for a positive feedback)

# **Steady-State Errors**

$$e_{ss} = \lim_{s \to 0} [s(1 - G_O(s))\theta_i(s)]$$
 (for an open-loop system)

$$e_{ss} = \lim_{s \to 0} [s \frac{1}{1 + G_o(s)} \theta_i(s)]$$
 (for the closed-loop system with a unity feedback)

$$e_{ss} = \lim_{s \to 0} \left[ s \frac{1}{1 + \frac{G_0(s)}{1 + G_0(s)[H(s) - 1]}} \theta_i(s) \right] \text{ (if the feedback H(s) $\neq 1$)}$$

$$e_{ss} = \lim_{s \to 0} \left[ -s \cdot \frac{G_2(s)}{1 + G_2(s)G_1(s)} \cdot \theta_d \right]$$
 (if the system subjects to a disturbance input)

state – space matrices for a second – order system 
$$\frac{bo}{(s^2 + a1s + ao)}$$

$$\frac{{\omega_n}^2}{s^2 + 2 \Im \omega_n s + \omega_n^2}$$

# **Laplace Transforms**

A unit impulse function 1

A unit step function  $\frac{1}{s}$ 

A unit ramp function  $\frac{1}{s^2}$ 

# First order Systems

$$G(s) = \frac{\theta_o}{\theta_i} = \frac{G_{ss}(s)}{\tau s + 1}$$

$$\tau \left(\frac{d\theta_o}{dt}\right) + \theta_o = G_{ss}\theta_i$$

$$\theta_{\scriptscriptstyle O} = G_{\scriptscriptstyle SS}(1-e^{-t/ au})$$
 (for a unit step input)

$$\theta_{\scriptscriptstyle O} = AG_{\scriptscriptstyle SS}(1-e^{-t/\tau})$$
 (for a step input with size A)

$$\theta_{o}(t) = G_{ss}(\frac{1}{\tau})e^{-(t/\tau)}$$
 (for an impulse input)

## **Second-order systems**

$$\frac{d^2\theta_o}{dt^2} + 2\zeta\omega_n \frac{d\theta_o}{dt} + \omega_n^2\theta_o = b_o\omega_n^2\theta_i$$

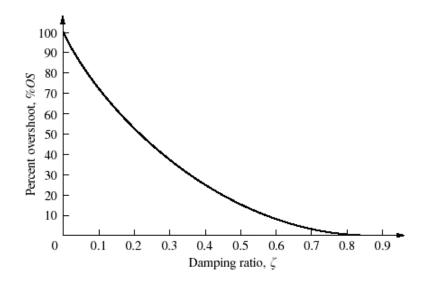
$$G(s) = \frac{\theta_o(s)}{\theta_i(s)} = \frac{b_o \omega_n^2}{s^2 + 2\zeta \omega_n s + \omega_n^2}$$

$$\omega_d t_r = 1/2\pi$$
  $\omega_d t_p = \pi$ 

P.O. = exp
$$(\frac{-\zeta\pi}{\sqrt{(1-\zeta^2)}}) \times 100\%$$

$$t_s = \frac{4}{\zeta \omega_n}$$
  $\omega_d = \omega_n \sqrt{(1-\zeta^2)}$ 

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$$h_f = \frac{\Delta P}{\rho g}$$

$$h_f = \frac{\Delta P}{\rho g}$$
 
$$h_f = \frac{4fLV^2}{2gD}$$

$$f = \frac{16}{R_e}$$

$$f = \frac{0.079}{R_e^{0.25}}$$

$$F = \dot{m} imes (V_{
m exit} - V_{
m jet})$$

$$\eta_{ ext{propulsive}} = rac{2v_0}{v_0 + v_e}$$

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Table 4.1 Laplace t	ransforms	LAPLACE TRANSFORMS 111
Laplace transform	Time function	Description of time function
1		A unit impulse
1 <u>1</u> \$		A unit step function
e=st;   S		A delayed unit step function
$\frac{1-e^{-st}}{s}$		A rectangular pulse of duration T
$\frac{1}{\overline{n^2}}$	t	A unit slope ramp function
$\frac{1}{s^2}$ $\frac{1}{s^3}$	$\frac{t^2}{2}$	
$\frac{1}{s+a}$	2 e-ai	Exponential decay
$\frac{s+a}{(s+a)^2}$	$te^{-at}$	Exponential decay
	$t^2 e^{-at}$	
$\frac{2}{(s+a)^3}$		
$\frac{a}{s(s+a)}$	$1 - e^{-at}$	Exponential growth
$\frac{a}{s^2(s+a)}$	$t - \frac{(1 - e^{-at})}{a}$	
$\frac{a^2}{s(s+a)^2}$	$1 - e^{-at} - ate^{-at}$	
$\frac{s}{(s+a)^2}$	$(1-at)\mathrm{e}^{-at}$	
$\frac{1}{(s+a)(s+b)}$	$\frac{e^{-at} - e^{-bt}}{b - a}$	
$\frac{ab}{s(s+a)(s+b)}$	$1 - \frac{b}{b - a} e^{-at} + \frac{a}{b - a} e^{-bt}$	
$\frac{1}{(s+a)(s+b)(s+c)}$	$\frac{e^{-at}}{(b-a)(c-a)} + \frac{e^{-bt}}{(c-a)(a-b)} + \frac{e^{-ct}}{(a-c)(b-c)}$	
$\frac{\omega}{s^2 + \omega^2}$	$\sin \omega t$	Sine wave
$\frac{s}{s^2 + \omega^2}$	COS ω <i>f</i>	Cosine wave
$\frac{\omega}{(s+a)^2+\omega^2}$	$e^{-at} \sin \omega t$	Damped sine wave
$\frac{s+a}{(s+a)^2+\omega^2}$	$e^{-at}\cos\omega t$	Damped cosine wave
$\frac{\omega^2}{s(s^2+\omega^2)} = \frac{1}{s(s^2+\omega^2)}$	$1-\cos\omega t$	
$\frac{\omega^2}{s^2 + 2\zeta\omega s + \omega^2}$	$\frac{\omega}{\sqrt{(1-\zeta^2)}}e^{-\zeta\omega t}\sin\left[\omega\sqrt{(1-\zeta^2)t}\right]$	
$\widetilde{s(s^2+2\zeta\omega s+\omega^2)}$	$1 - \frac{1}{\sqrt{(1-\zeta^2)}} e^{-\zeta\omega t} \sin\left[\omega\sqrt{(1-\zeta^2)}t + \phi\right]$	
with $\xi < 1$	with $\zeta = \cos \varphi$	

Table 15.1 z-transforms

Sampled f(t), sampling period T	F(z)
Unit impulse, $\delta(t)$	1
Unit impulse delayed by $kT$	$z^{-k}$
Unit step, $u(t)$	$\frac{z}{z-1}$
Unit step delayed by $kT$	$\frac{z}{z^k(z-1)}$
Unit ramp, t	$\frac{Tz}{(z-1)^2}$
$t^2$	$\frac{T^2z(z+1)}{(z-1)^3}$
$e^{-at}$	$\frac{z}{z - e^{-aT}}$
$1 - e^{-at}$	$\frac{z(1 - e^{-aT})}{(z - 1)(z - e^{-aT})}$
t e <sup>-at</sup>	$\frac{Tz e^{-aT}}{(z - e^{-aT})^2}$
$e^{-at} - e^{-bt}$	$\frac{(e^{-aT} - e^{-bT})z}{(z - e^{-aT})(z - e^{-bT})}$
sin $\omega t$	$\frac{z\sin\omega T}{z^2 - 2z\cos\omega T + 1}$
$\cos \omega t$	$\frac{z(z-\cos\omega T)}{z^2-2z\cos\omega T+1}$
$e^{-at}\sin\omega t$	$\frac{z e^{-aT} \sin \omega T}{z^2 - 2z e^{-aT} \cos \omega T + e^{-2}}$
$e^{-at}\cos\omega t$	$\frac{z(z - e^{-aT}\cos\omega T)}{z^2 - 2z e^{-aT}\cos\omega T + e^{-2}}$

Table 15.2 z-transforms

f[k]	f[0], f[1], f[2], f[3],	F(z)
1u[k]	1, 1, 1, 1,	$\frac{z}{z-1}$
$a^k$	$a^0, a^1, a^2, a^3, \dots$	$\frac{z}{z-a}$
k	0, 1, 2, 3,	$\frac{z}{(z-1)^2}$
ka <sup>k</sup>	$0, a^1, 2a^2, 3a^3, \dots$	$\frac{az}{(z-a)^2}$
ka <sup>k-1</sup>	$0, a^0, 2a^1, 3a^2, \dots$	$\frac{z^2}{(z-a)^2}$
$e^{-ak}$	$e^{0}$ , $e^{-a}$ , $e^{-2a}$ , $e^{-3a}$ ,	$\frac{z}{z-e^{-a}}$