OCD16

UNIVERSITY OF BOLTON

OFF CAMPUS DIVISION

WESTERN INTERNATIONAL COLLEGE

BENG (HONS) CIVIL ENGINEERING

SEMESTER ONE EXAMINATION 2023/24

GEOTECHNICAL ENGINEERING

MODULE NO: CIE6020

Date: Saturday 06 January 2024

Time:10:00 AM – 1:00 PM

INSTRUCTIONS TO CANDIDATES:

There are <u>FIVE</u> questions on this paper.

Answer any <u>FOUR</u> questions.

All questions carry equal marks.

Marks for parts of questions are shown in brackets.

This examination paper carries a total of 100 marks.

Formula sheet / supplementary information is provided on page 16

All working must be shown. A numerical solution to a question obtained by programming an electronic calculator will not be accepted.

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Question 1

(a) A 400 mm diameter concrete pile is driven for a 10.00 m into layered soils and the details are as follows:

Loose sand	2.50m thick	(γ=17.0 kN/m³; N = 18)
Dense sand	2.0m thick	(γ = 20.0 kN/m³; N = 21)
Compact Sand	10.0m thick	(γ _{sat} = 22.0 kN/m ³ ; N = 33)

The water table is at 4.50m from ground level. Determine the safe working load of this pile by adopting factors of safety of 1.50 and 2.50 for the shaft and end bearing resistance respectively.

Use Figures Q1-1, Q1-2, and Q1-3 on Pages 12 to 13 and the formulae provided in the supplementary sheet. (12 marks)

- (b) In a site of almost similar conditions, instead of dense sand if there is a layer of soft clay for 2m (γ = 18.0 kN/m³), what might be the possible effect on the safe load-bearing capacity of the pile? Justify your findings with the help of suitable sketches/equations. (6 marks)
- (c) A large diameter under-reamed bored pile is to be installed in stiff clay with an undrained shear strength value of 215 kN/m². The main shaft of the pile is 1.2m diameter and the base of the under ream is 3.5m diameter with a height of 2.5m. The total length of the pile from the ground level to the base of the under-ream is 15 m. Determine the working load of the pile in MN, assuming the following factors for adhesion, $\alpha = 0.3$ and end bearing N c = 9.0. Apply a factor of safety of 3.0 to the base load. Full mobilisation of shaft adhesion can be assumed. Clearly state all assumptions made in your analysis. (7 marks)

Total 25 marks

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Question 2

- (a) A reinforced concrete gravity wall, 1.5m wide at its top and 2m wide at its base
 - is resting upon and also retains 6.0m of soil. Assume the water table is at greater depth.

A cross-section through the wall is shown in Figure Q2 on Page 4.

Other relevant parameters are:

- **Soil 1:** Bulk Unit weight 17.0 kN/m³ Effective friction angle φ = 18° Soil depth: 3m
- **Soil 2**: Bulk Unit weight 19.0 kN/m³ Effective friction angle φ[´]= 32° Soil depth: 2m

Surcharge : 15kN/m² on upper retained surface

Reinforced concrete Unit weight: 24 kN/m³

- (i) Sketch the earth pressure diagram for the retained soil, labelling all relevant values. Determine, by calculation, the resultant thrust acting on the back of the retaining wall.
 (17 marks)
- (ii) Determine the height of the resultant thrust above the base of the retaining wall and hence determine the Factor of Safety against overturning (Ignore water pressures on the base of the foundation)
 (3 marks)

Question 2 continued over... Please turn the page

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Question 2 continued...

(iii) What are the advantages and disadvantages of using an "embedded secant pile wall" instead of a gravity retaining wall in the above scenario? Ensure that your answer discusses construction practicality as well as technical aspects concerning the development of earth pressures on either side of the embedded wall. (5 marks)



Total 25 marks

Question 3

(a) A 7m height cutting is excavated in a thick stratum of saturated clay with the following properties:

Question 3 continued over... Please turn the page

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Question 3 continued...

Saturated Unit weight, $\bigcirc_{sat} = 20 \text{ kN/m}^3$ Strength parameters with respect to effective stress, C' = 20 kN/m²,)' = 30⁰

A trial slip surface of radius 12m and sector angle 71⁰ is dividing the sector into 6 slices as shown in **Figure Q3-1** on **Page 14**.

- i) Complete the table shown in Table Q3 on Page 15 and hence determine the long-term factor of safety, F, of the trial slip surface using Swedish (Fellenius) analysis.
 (13 marks)
- ii) In the above scenario, if earthquake forces are expected what factors should be considered for determining the factor of safety? (2 marks)
- (b) Explain why regular inspections of the ground behind the crest is advisable when a cutting is being excavated. Explain your answer with the help of diagram. (5 marks)

(c) A cutting in saturated clay has a vertical height of 8.0m. Hard bedrock is located at a depth of 4.0m below the floor of the cutting. The clay has the following properties;

Undrained cohesion, $C_u = 40.0 \text{kN/m}^2$ Undrained angle of friction, $\varphi u = 0^\circ$

> Question 3 continued over... Please turn the page

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Question 3 continued...

Unit weight, $\gamma = 19.0$ kN/m³

Using Figure Q3-2 on Page 6, determine the factor of safety against short-term failure,

if the cutting has a side slope of 10^{0.}



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Question 4

(a) **Figure Q4-1** on **page 7** shows a layer of sand 6 m thick lies above a layer of clay soil. The water table is at a depth of 2 m below the ground surface. The void ratio of the sand layer is 0.6 and the degree of saturation of the sand layer above the water table is 40%. The void ratio of the clay layer is 0.7. Assume specific gravity of the sand and clay soil as 2.65 and 2.7. Consider the unit weight of water $\gamma_w = 9.81 \ kN/m^3$.



Question 4 continued over... Please turn the page

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Question 4 continued...

(b) A foundation 2 m x 2 m square is installed 1.2 m below the surface of a uniform sandy gravel. The strength parameters with respect to effective stress are c' = 0 and φ' = 30°. Take the unit weight of water $\gamma_w = 9.81 \ kN/m^3$. Consider the following soil densities.

$$\gamma = 19.2kN/m^3$$
$$\gamma_{sat} = 21.4kN/m^3$$

 i) Calculate the ultimate bearing capacity of soil when water table is at a depth of 6m from ground level.

(3 marks)

(ii) Determine the safe bearing capacity of soil when the water table is level with the foundation base. Choose a minimum FOS from **Table Q4 a** on **page 9**.

(6 marks)

(iii) Calculate the ultimate bearing capacity of soil when water table rises to0.5 m below the ground level.

(4 marks)

NOTE: Clearly state any assumptions made in your calculations to determine the safe bearing capacity. Use **Tables Q4 b and Q4 c** on **pages 9-10** and the formulae provided on **Supplementary Information**.

Total 25 marks

Question 4 continued over... Please turn the page

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Question 4 continued ...

Table Q4 a: Minimum factors of safety for shallow foundation

Category	Characteristics of	Extent of s	ite investigation	Typical Structure
	category	Thoroug	Limited	
		h		
	Maximum design load:			Railway bridges
	likely to occur often.			warehouses
А	Consequences of	3.0	4.0	Blast furnaces
	failure: disastrous			Reservoir
				embankments
				Retaining walls /
				silos
	Maximum design load:			Highway bridges
	May occur			Light industrial
В	occasionally.	2.5	3.5	Public buildings
	Consequences of			
	failure: serious			
	Maximum design load:			Apartments Office
С	Unlikely to occur.	2.0	3.0	buildings.

Table Q4 b: Shape Factors

Shape of footing	Sc	Sq	S _Y
Strip	1.0	1.0	1.0
Rectangle	$1.0 + (B/L)(N_q/N_c)$	$1.0 + (B/L) \tan \phi'$	1.0 - (B/L) 0.4
Circle or Square	$1.0 + (N_q / N_c)$	$1.0 + \tan \phi'$	0.6

Question 4 continued over... Please turn the page

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Question 4 continued ...

φ	Nc	Nq	Νγ
0	5.14	1.0	0
1	5.4	1.1	0
2	5.6	1.2	0
3	5.9	1.3	0
4	6.2	1.4	0
5	6.5	1.6	0.1
6	6.8	1.7	0.1
7	7.2	1.9	0.2
8	7.5	2.1	0.2
9	7.9	2.3	0.3
10	8.4	2.5	0.4
11	8.8	2.7	0.5
12	9.3	3.0	0.6
13	9.8	3.3	0.8
14	10.4	3.6	1.0
15	11.0	3.9	1.2
16	11.6	4.3	1.4
17	12.3	4.8	1.7
18	13.1	5.3	2.1
19	13.9	5.8	2.5
20	14.8	6.4	3.0
21	15.8	7.1	3.5
22	16.9	7.8	4.1
23	18.1	8.7	4.9
24	19.3	9.6	5.7
25	20.7	10.7	6.8
26	22.3	11.9	7.9
27 /	23.9	13.2	9.3
28	25.8	14.7	10.9
29	27.9	16.4	12.8
30	30.1	18.4	15.1
31	32.7	20.6	17.7
32	35.5	23.2	20.8
33	38.0	20.1	24.4
34	42.2	29.4	20.0
35	40.1	33.3	33.9
30	50.6	37.8	40.0
31	55.0	42.9	41.4
38	01.4	46.9	2.00
39	07.9	0.00	00.8
40	/5.3	04.2	79.5

Table Q4 c: Bearing capacity factors

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Question 5

- (a) A saturated soil has a compression index of 0.25. The void ratio of this soil at a stress of 10 kN/m^2 is 2.02 and the permeability is 3.4 x 10⁷ mm/sec. Calculate:
 - (i) Change in void ratio, Coefficient of compressibility and coefficient of volume compressibility, if the stress is increased to $19 kN/m^2$.

(4 marks)

(ii) Settlement of the above scenario, if the soil stratum is 5 m thick.

(3 marks)

(iii) Time required for 40% consolidation if drainage is one way.

(5 marks)

(b)

(i) A clay layer 4 m thick is subjected to a pressure of $55 kN/m^2$. If the layer has a double drainage and undergoes 50% consolidation in one year, determine the coefficient of consolidation. Take $T_v = 0.196$. If the coefficient of permeability is 0.020 m/yr, determine the settlement in one year and rate of flow of water per unit area in one year.

(8 marks)

 (ii) Illustrate the pressure – void ratio relationship for a typical sand under one-dimensional compression.

> (5 marks) Total 25 marks

Question 5 continued over... Please turn the page

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Question 5 continued...



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Question 4 continued...

TO BE HANDED IN WITH ANSWER BOOK

CANDIDATE NUMBER

Table Q3

	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(I)
Slice	b	h	<	hw	I	ul	W	sin∢	cos〈	Wcos〈	Wcos∢-ul	Wsin∢
No:	(m)	(m)	(deg)	(m)	(b/cos⟨)		kN					
1	2.0	0.9	0	0.9								
2	2.0	2.4	9	2.4								
3	2.0	3.6	19	3.6								
4	2.0	4.5	29	4.5								
5	2.0	4.0	42	4.0		•						
6	2.0	1.80	55	1.0								
										©		

END OF QUESTIONS

Please turn the page (for Supplementary Geotechnical Information)

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Supplementary Geotechnical Information

Density kg/m³

 $\rho_b = \rho_w \, \frac{(G_s + eS_r)}{1 + e}$

$$\rho_b = \rho_w \, G_s \frac{(1+w)}{1+e}$$

 $\boldsymbol{3} \qquad \qquad \rho_b = \frac{\rho_w \, G_s}{1+e}$

$$\boldsymbol{4} \qquad \qquad \rho_{sat} = \rho_w \, \frac{(G_s + e)}{1 + e}$$

Unit weight kN/m³

$$\gamma_b = \gamma_w \frac{(G_s + eS_r)}{A + e}$$
$$\gamma_b = \gamma_w G_s \frac{(1 + w)}{1 + e}$$
$$\gamma_d = \frac{\gamma_w G_s}{1 + e}$$
$$\gamma_{sat} = \gamma_w \frac{(G_s + e)}{1 + e}$$

Terzaghi's equation:

$$q_u = CN_cS_c + \gamma DN_qS_q + 0.5\gamma BN_\gamma S_\gamma$$

$$q_{net \ safe} = \frac{q_u - \gamma D}{F} + \gamma D$$

$$\gamma_{sub} = \gamma_{sat} - \gamma_w$$
, when water table is affecting bearing capacity

$$C_c = \frac{\Delta e}{\log_{10}(\frac{\sigma_1}{\overline{\sigma_0}})}$$

$$a_{v} = \frac{\Delta e}{\Delta \underline{\sigma}}$$

$$m_v = \frac{a_v}{(1+e_0)}$$

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$$m_{v} = \frac{\Delta e}{(1 + e_{0})} \cdot \frac{1}{\Delta \sigma}$$

$$s = \frac{H \cdot C_{c}}{(1 + e_{0})} \log_{10} \left(\frac{\sigma_{0} + \Delta \sigma}{\sigma_{0}}\right)$$

$$= \frac{H \cdot C_{c}}{(1 + e_{0})} \log_{10} \left(\frac{\sigma_{1}}{\sigma_{0}}\right)$$

$$S_{f} = m_{v} H_{0} \Delta \underline{\sigma}$$

$$C_{v} = \frac{k}{m_{v} \cdot \gamma_{w}}$$

$$C_{v} = \frac{T_{v} d^{2}}{t}$$
Time factor $T = \frac{C_{0} \cdot t}{H^{2}}$
when U < 60%, $T = (-0.9332 \log_{10}(1 - U) - 0.0851)$

$$\Delta H = m_{v} \Delta \sigma H_{o}$$
Earth Pressure:
$$k_{c} = \frac{1 - \sin \phi}{1 + \sin \phi}$$
Pile Foundations.

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$$Q_u = Q_s + Q_b$$

For Cohesive Soil, $Q_b = C_u N_c A_b$, $Q_s = \alpha . \underline{C_u}^- A_s$

For Cohesionless soil, $Q_b = N_q \cdot \sigma'_v \cdot A_b$, $Q_s = K_s \cdot \tan \tan \delta \cdot \sigma_v^{-} \cdot A_s$

$$\sigma_v = \gamma . D$$

Slope Stability,

F

 $(Wcos\alpha - ul)tan\phi$ $C_u.R.\theta_c.\left(\frac{\pi}{180}\right)$ $+\Sigma$

Wsinα

END OF PAPER