

[ENG16]

UNIVERSITY OF BOLTON

SCHOOL OF ENGINEERING

BEng (HONS) CIVIL ENGINEERING

SEMESTER ONE EXAMINATION 2023/2024

**GEOTECHNICAL ENGINEERING & GROUND
IMPROVEMENT**

MODULE NO: CIE6003

Date: Wednesday 10th January 2024

Time: 10:00am – 1:00pm

INSTRUCTIONS TO CANDIDATES:

There are **FOUR** questions.

Answer **ALL FOUR** questions.

All questions carry equal marks.

Marks for parts of questions are shown in brackets.

Supplementary Geotechnical Information / Formulas are provided on p. 10 to 12.

Question 1

- a) Produce a sketch to illustrate the relationship between the three different types of lateral earth pressure and the wall movement. With reference to your sketch, explain what happens when there is no movement of the wall, movement of the wall towards the soil and movement of the wall away from soil. In relation to strain, also explain when the minimum P_a and maximum P_p are achieved.

(5 marks)

- b) A concrete retaining wall retains two layers of soil (Figure Q1). With depth the sequence includes: 4.0m of soil 1 and 5.0m of soil 2. Plot the active stress and determine the total thrust and point (line) of action for the wall shown below. The properties of the materials are summarised below:

$$q = 40.0 \text{ kN/m}^2$$

Soil 1:

$$z_1 = 4.0 \text{ m}$$

$$\phi_1 = 27^\circ$$

$$\gamma_1 = 17.41 \text{ kN/m}^3$$

Soil 2:

$$z_2 = 5.0 \text{ m}$$

$$\phi_2 = 31^\circ$$

$$\gamma_2 = 21.5 \text{ kN/m}^3$$

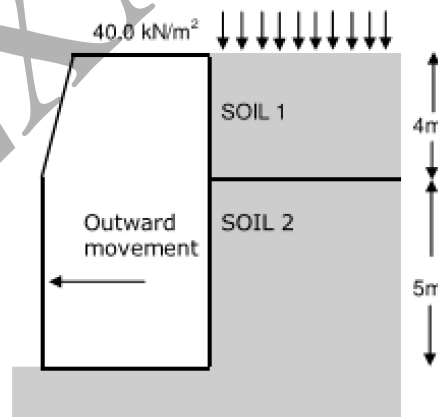


Figure Q1

(20 marks)

Total 25 marks

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Question 2

- a) For slope stability of an embankment, what are the main factors that influence slope stability? And what makes a slope globally stable? Explain your answer. **(5 marks)**
- b) An embankment made from clay is to be constructed upon the ground surface (See Figure Q2). The completed embankment can be assumed to be homogenous and thus will possess constant density and constant shear strength throughout its mass. Determine the factor of safety in the short term (undrained state). Area and angle of base for each slice is calculated in Table 1 below.

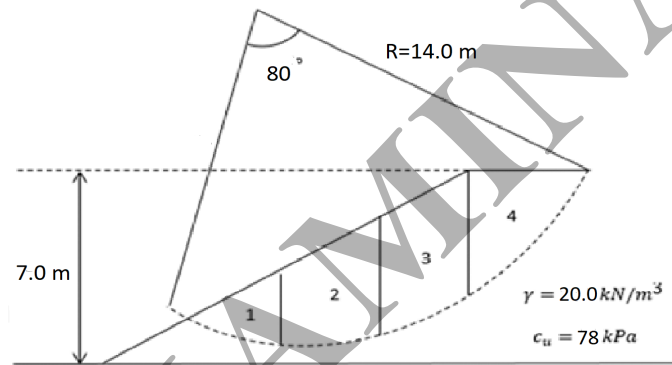


Figure Q2

| Slice No. | Area (m ²) A | Angle of base (α°) |
|-----------|--------------------------|----------------------------------|
| 1 | 3.5 | -5.0 |
| 2 | 7.5 | 14.0 |
| 3 | 11.0 | 30.0 |
| 4 | 7.0 | 45.0 |

Table 1

(20 marks)

Total 25 marks

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Question 3

a) A wide embankment, 5m high, is to be constructed over a 10m thick layer of very soft to soft clay ($m_v = 0.6\text{m}^2/\text{MN}$, $c_v = 4\text{m}^2/\text{yr}$). This clay overlies a relatively impermeable layer of mudstone. The embankment is to be formed by compacting granular material to a bulk unit weight of $21\text{kN}/\text{m}^3$.

i) Calculate the total consolidation settlement within the clay layer.

(4 marks)

ii) If “finishing works” can be commenced on top of the embankment as soon as $<35\text{mm}$ of consolidation settlement of the very soft clay layer remains to be achieved, then calculate the earliest time that “finishing works” can be commenced.

(4 marks)

b) If 250mm diameter vertical sand drains are used then determine the square grid spacing of drains required to achieve the same settlement requirements as stipulated in Q3 a) ii) – ie. only 35mm of consolidation settlement remaining within 3-months.

NOTE: Assume $c_h = 9\text{m}^2/\text{yr}$ and

Fig Q3 in page 5 and Table Q3 in page 6 are provided for the solution of this question.

(13 marks)

c) Where a section of proposed new high speed rail track is required to be constructed over 6m of loose granular deposits, propose and briefly evaluate **FOUR** ground improvement options that may be considered to ensure a stable platform is achieved. Ensure that you evaluate the advantages and limitations of each option from a geotechnical perspective.

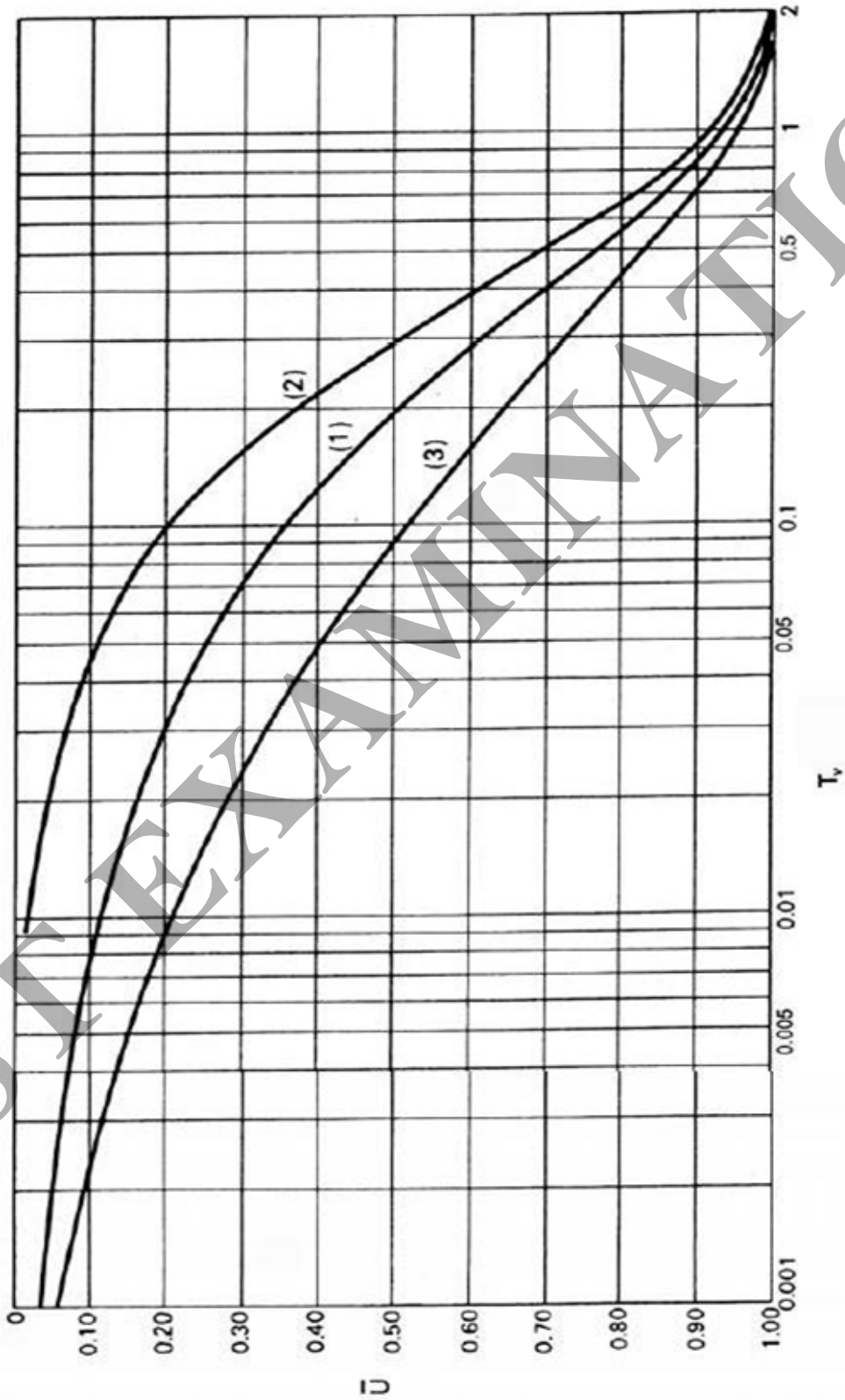
(4 marks)

Total 25 marks

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Fig. Q3



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Table Q3

| Degree of consolidation U_r (%) | Dimensionless Time Factor, T_r | | | | | | | | | | |
|--------------------------------------|----------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | n=5 | 10 | 15 | 20 | 25 | 30 | 40 | 50 | 60 | 80 | 100 |
| 10 | 0.012 | 0.021 | 0.026 | 0.030 | 0.032 | 0.035 | 0.039 | 0.042 | 0.044 | 0.048 | 0.051 |
| 20 | 0.026 | 0.044 | 0.055 | 0.063 | 0.069 | 0.074 | 0.082 | 0.088 | 0.092 | 0.101 | 0.107 |
| 30 | 0.042 | 0.070 | 0.088 | 0.101 | 0.110 | 0.118 | 0.131 | 0.141 | 0.149 | 0.162 | 0.172 |
| 40 | 0.060 | 0.101 | 0.125 | 0.144 | 0.158 | 0.170 | 0.188 | 0.202 | 0.214 | 0.232 | 0.246 |
| 50 | 0.081 | 0.137 | 0.170 | 0.195 | 0.214 | 0.230 | 0.255 | 0.274 | 0.290 | 0.315 | 0.334 |
| 55 | 0.094 | 0.157 | 0.197 | 0.225 | 0.247 | 0.265 | 0.294 | 0.316 | 0.334 | 0.363 | 0.385 |
| 60 | 0.107 | 0.180 | 0.226 | 0.258 | 0.283 | 0.304 | 0.337 | 0.362 | 0.383 | 0.416 | 0.441 |
| 65 | 0.123 | 0.207 | 0.259 | 0.296 | 0.325 | 0.348 | 0.386 | 0.415 | 0.439 | 0.477 | 0.506 |
| 70 | 0.137 | 0.231 | 0.289 | 0.330 | 0.362 | 0.389 | 0.431 | 0.463 | 0.490 | 0.532 | 0.564 |
| 75 | 0.162 | 0.273 | 0.342 | 0.391 | 0.429 | 0.460 | 0.510 | 0.548 | 0.579 | 0.629 | 0.668 |
| 80 | 0.188 | 0.317 | 0.397 | 0.453 | 0.498 | 0.534 | 0.592 | 0.636 | 0.673 | 0.730 | 0.775 |
| 85 | 0.222 | 0.373 | 0.467 | 0.534 | 0.587 | 0.629 | 0.697 | 0.750 | 0.793 | 0.861 | 0.914 |
| 90 | 0.270 | 0.455 | 0.567 | 0.649 | 0.712 | 0.764 | 0.847 | 0.911 | 0.963 | 1.046 | 1.110 |
| 95 | 0.351 | 0.590 | 0.738 | 0.844 | 0.926 | 0.994 | 1.102 | 1.185 | 1.253 | 1.360 | 1.444 |
| 99 | 0.539 | 0.907 | 1.135 | 1.298 | 1.423 | 1.528 | 1.693 | 1.821 | 1.925 | 2.091 | 2.219 |

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Question 4

- a) A pad foundation, 3.0m square is to be located at a depth of 2.0m in a uniform bearing stratum of firm clay. The clay soil properties are;

| | |
|--------------------------------|--------------------------------|
| Bulk unit weight | $\gamma = 20.0 \text{ kN/m}^3$ |
| Depth of Foundation | $D_f = 2.0 \text{ m}$ |
| With respect to Total Stresses | $c = 40.0 \text{ kN/m}^2$ |
| | $\Phi = 30^\circ$ |

Determine the allowable bearing capacity (q_{all}), the net allowable bearing capacity ($q_{(net)all}$), the allowable load (Q_{all}), and the net allowable load ($Q_{(net)all}$) that the foundation can support in the short-term (in kN). **Use the formulae provided on page 11 and also Figure Q4 in page 8 and/or Table Q4 in page 9 (if appropriate).**

Use Factor of Safety 2.5. State any assumptions made in your calculations.

(12 marks)

- b) A bored pile (15m long and 600mm diameter) is to be installed into the following soil profile;

| Depth m | Description | Unit Weight kN/m ³ | c_u kN/m ² | Adhesion Factor α |
|------------|--------------------------|----------------------------------|----------------------------|-----------------------------|
| 0 – 4 | Soft CLAY | 21.0 | 30.0 | 0.52 |
| 4 – 8 | Firm to stiff CLAY | 22.0 | 75.0 | 0.48 |
| 8 - 30 | Stiff to very stiff CLAY | 22.5 | 180.0 | 0.42 |

Determine the safe load carrying capacity of the pile (in kN). State any assumptions made in your calculations

(13 marks)

Total 25 marks

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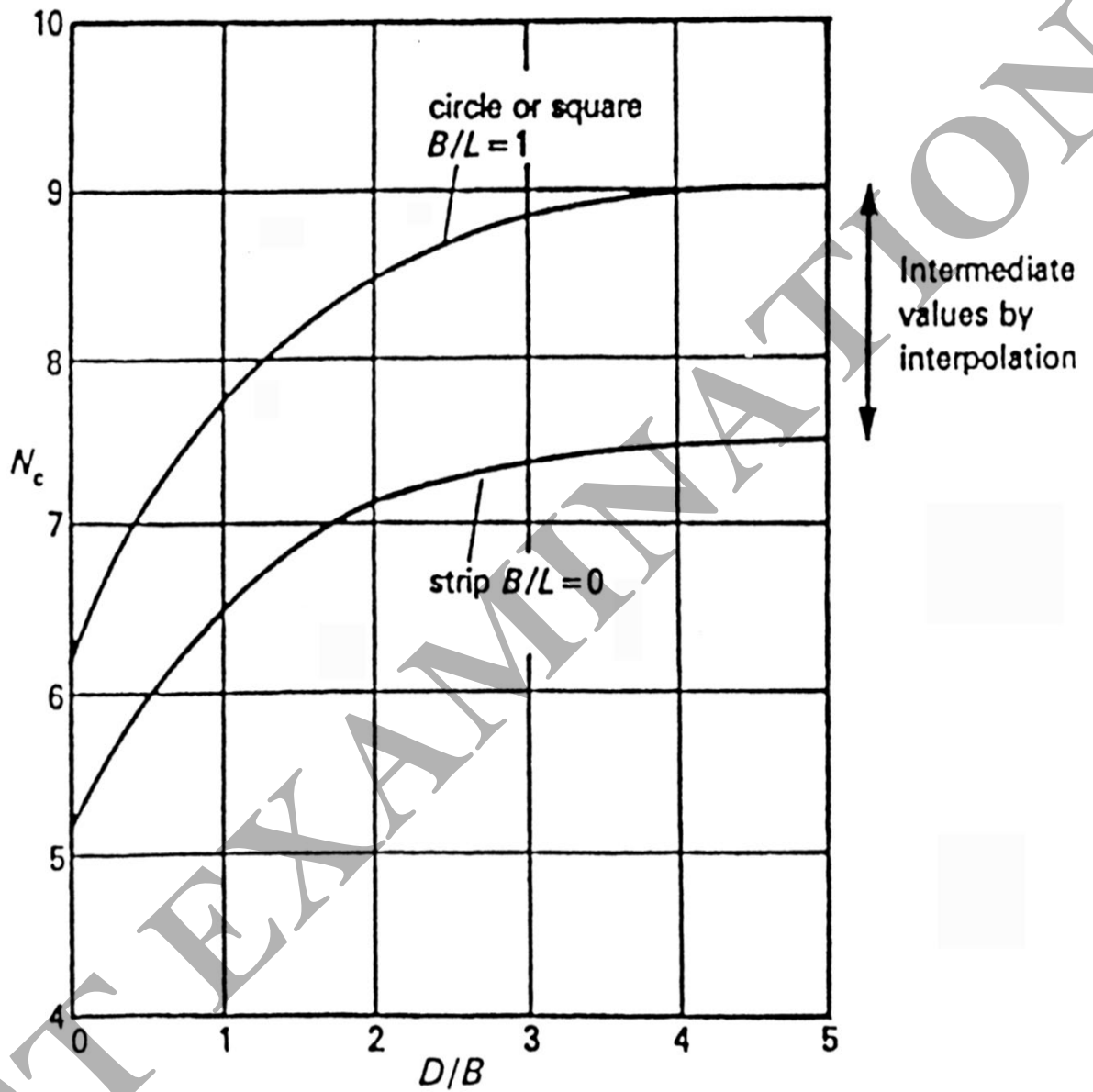


Figure Q4

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| ϕ | N_c | N_q | N_γ |
|--------|-------|-------|------------|
| 0 | 5.14 | 1.0 | 0 |
| 1 | 5.4 | 1.1 | 0 |
| 2 | 5.6 | 1.2 | 0 |
| 3 | 5.9 | 1.3 | 0 |
| 4 | 6.2 | 1.4 | 0 |
| 5 | 6.5 | 1.6 | 0.1 |
| 6 | 6.8 | 1.7 | 0.1 |
| 7 | 7.2 | 1.9 | 0.2 |
| 8 | 7.5 | 2.1 | 0.2 |
| 9 | 7.9 | 2.3 | 0.3 |
| 10 | 8.4 | 2.5 | 0.4 |
| 11 | 8.8 | 2.7 | 0.5 |
| 12 | 9.3 | 3.0 | 0.6 |
| 13 | 9.8 | 3.3 | 0.8 |
| 14 | 10.4 | 3.6 | 1.0 |
| 15 | 11.0 | 3.9 | 1.2 |
| 16 | 11.6 | 4.3 | 1.4 |
| 17 | 12.3 | 4.8 | 1.7 |
| 18 | 13.1 | 5.3 | 2.1 |
| 19 | 13.9 | 5.8 | 2.5 |
| 20 | 14.8 | 6.4 | 3.0 |
| 21 | 15.8 | 7.1 | 3.5 |
| 22 | 16.9 | 7.8 | 4.1 |
| 23 | 18.1 | 8.7 | 4.9 |
| 24 | 19.3 | 9.6 | 5.7 |
| 25 | 20.7 | 10.7 | 6.8 |
| 26 | 22.3 | 11.9 | 7.9 |
| 27 | 23.9 | 13.2 | 9.3 |
| 28 | 25.8 | 14.7 | 10.9 |
| 29 | 27.9 | 16.4 | 12.8 |
| 30 | 30.1 | 18.4 | 15.1 |
| 31 | 32.7 | 20.6 | 17.7 |
| 32 | 35.5 | 23.2 | 20.8 |
| 33 | 38.6 | 26.1 | 24.4 |
| 34 | 42.2 | 29.4 | 28.8 |
| 35 | 46.1 | 33.3 | 33.9 |
| 36 | 50.6 | 37.8 | 40.0 |
| 37 | 55.6 | 42.9 | 47.4 |
| 38 | 61.4 | 48.9 | 56.2 |
| 39 | 67.9 | 56.0 | 66.8 |
| 40 | 75.3 | 64.2 | 79.5 |

Table Q4

END OF QUESTIONS

Supplementary Geotechnical Information / Formulas follow over the page

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Supplementary Geotechnical Information

Retaining Walls (Q1)

$$P_A = K_A(\gamma z + q) - 2c\sqrt{K_A}$$

$$P_P = K_P(\gamma z + q) + 2c\sqrt{K_P}$$

$$K_A = \frac{1 - \sin \phi}{1 + \sin \phi} = \tan^2 \left(45 - \frac{\phi}{2} \right)$$

$$K_P = \frac{1 + \sin \phi}{1 - \sin \phi} = \tan^2 \left(45 + \frac{\phi}{2} \right)$$

(P_A , P_P , K_A and K_P are the active and passive pressures and coefficients respectively, z is the depth, γ is the unit weight and q is the surcharge)

Slope stability (Q2)

$$F = \frac{c_u R \theta}{\sum T}$$

$$F = \frac{c_u R \theta}{\sum W \sin \alpha}$$

(R is the radius of the slip circle, θ is the included angle, α is the base angle and W is the weight of soil for each slice)

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3-d Consolidation (Q3)

$$\Delta h = \Delta \delta' m_v H$$

$$\Delta \delta' = \gamma z$$

$$(1 - U) = (1 - U_v)(1 - U_r)$$

$$T_v = c_v t / d^2 \quad T_r = c_h t / 4R^2$$

$R = 0.564 S$ for square grid pattern

$$n = R/r_d$$

Shallow Foundations and Piles (Q4)

q_{all} = allowable bearing capacity = q_u / F

$q_{net(all)}$ = net allowable bearing capacity = $(q_u - \gamma D) / F$

c_u soil ($\phi_u = 0$)

Skempton : $q_f = c_u N_c + \gamma D$

c, ϕ soil

Terzaghi: $q_u = c N_c s_c + \gamma D N_q s_q + 0.5 B \gamma N_\gamma s_\gamma$

Where $N_c ; N_q ; N_\gamma ; s_c ; s_q ; s_\gamma$ are bearing capacity and shape factors

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| Shape of footing | s_c | s_q | s_γ |
|------------------|------------------------|------------------------|------------------|
| Strip | 1.0 | 1.0 | 1.0 |
| Rectangle | $1.0 + (B/L)(N_q/N_c)$ | $1.0 + (B/L)\tan\phi'$ | $1.0 - (B/L)0.4$ |
| Circle or square | $1.0 + (N_q/N_c)$ | $1.0 + \tan\phi'$ | 0.6 |

$$\text{Shaft Resistance } Q_s = \alpha c_u \pi d L$$

$$\text{Base Resistance } Q_b = c_u N_c \pi d^2 / 4$$

$$Q_{\text{safe}} = Q_b/3 + Q_s \quad \text{OR} \quad Q_{\text{safe}} = (Q_b + Q_s) / 2.5$$

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