

**UNIVERSITY OF BOLTON**

**SCHOOL OF ENGINEERING**

**BEng(Hons) MECHANICAL ENGINEERING**

**SEMESTER 1 EXAM 2022-23**

**ADVANCED THERMOFLUIDS AND CONTROL**  
**MODULE NUMBER: AME6015**

Date: Wednesday 11<sup>th</sup> January 2023

Time: 10:00 – 12:00

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**INSTRUCTIONS TO CANDIDATES:**

There are **SIX** questions.

Answer any **FOUR** questions.

All questions carry equal marks.

Marks for parts of questions are shown in brackets.

This examination paper carries a total of 100 marks.

Formulae sheet is attached at the end of the paper for reference.

All working must be shown. A numerical solution to a question obtained by programming an electronic calculator will not be accepted.

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 Advanced Thermo-fluids and Control  
 Module No. AME 6015

### Question 1

A block diagram for a furnace temperature control system is shown in Figure Q1 below:

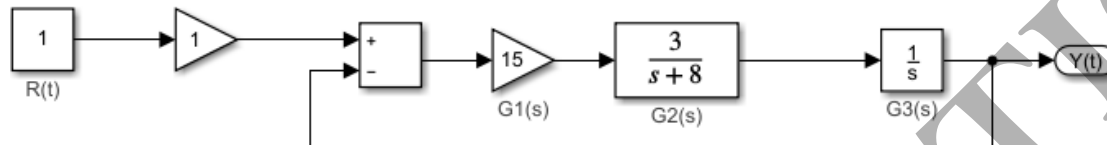


Figure Q1

Where,

$$G_1(s) = 15$$

$$G_2(s) = \frac{3}{s+8}$$

$$G_3(s) = \frac{1}{s}$$

- Determine the system damping ratio, natural frequency, damped frequency, and steady state gain. **[7 marks]**
- Determine the time domain response of the system,  $y(t)$ , to a unit impulse input,  $r(t)$ . **[6 marks]**
- For a unit step input, determine the system rise time, peak time, maximum percentage overshoot, and settling time for a 2% tolerance. **[6 marks]**
- If the input of  $r(t) = 90, t \geq 0$  and  $0, t \leq 0$  is applied, analyse the system steady state error. **[6 marks]**

**Total: 25 marks**

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### Question 2

A block diagram for a digital control system for a steam-turbine speed control is shown below in Figure Q2.

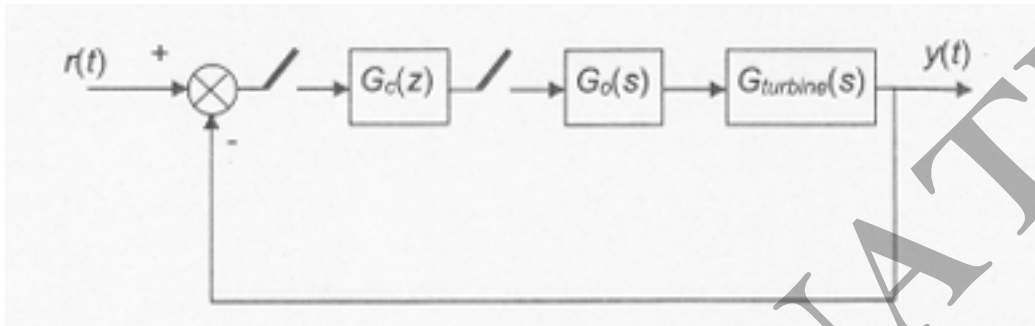


Figure Q2

Where,

The digital controller:  $G_c = K_p$

The zero-order-hold:  $G_o = \frac{1 - e^{-sT}}{s}$

The dynamics of the steam-turbine:  $G_{Turbine}(s) = \frac{0.5}{s+0.5}$

- Determine the closed-loop z-transfer function for the system. **[12 marks]**
- if the gain of the digital controller  $K_p = 10$ , determine the range of the sampling time interval  $T$  that will make the closed-loop control system stable. **[6 marks]**
- If the sampling frequency  $f = 20\text{kHz}$ , determine the range of controller gain  $K_p$  that will make the closed-loop system stable. **[7 marks]**

**Total: 25 marks**

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### Question 3

A dynamic system is shown in the block diagram below, Figure Q3(a),

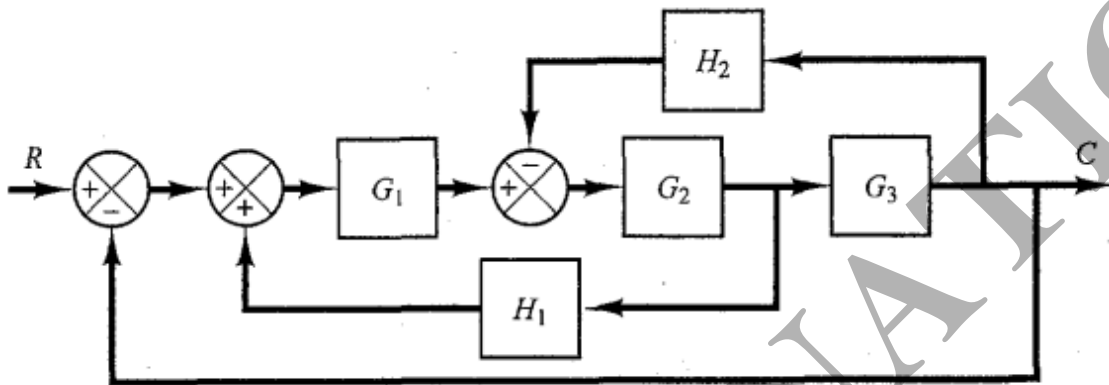


Figure Q3(a)

- a) Show how the block diagram in figure Q3(a) could be reduced to describe the output over the input  $C/R$ . **[6 marks]**
- b) From the Matlab graph shown in Q3(b) on the next page, estimate the gain and phase margins **[6 marks]**
- c) Sketch the magnitude and phase for the following functions.
- (i)  $G1(s) = \frac{10}{0.2s+1}$  **[2 marks]**
- (ii)  $G2(s) = \frac{2500}{s^2 + 80s + 2500}$  **[2 marks]**
- (iii)  $G3(s) = \frac{8}{s}$  **[2 marks]**
- d) Sketch the final result of  $G1(s)*G2(s)*G(s)$  and estimate the phase and gain margin. **[7 marks]**

Question 3 follows over the page...

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....Question 3 continued

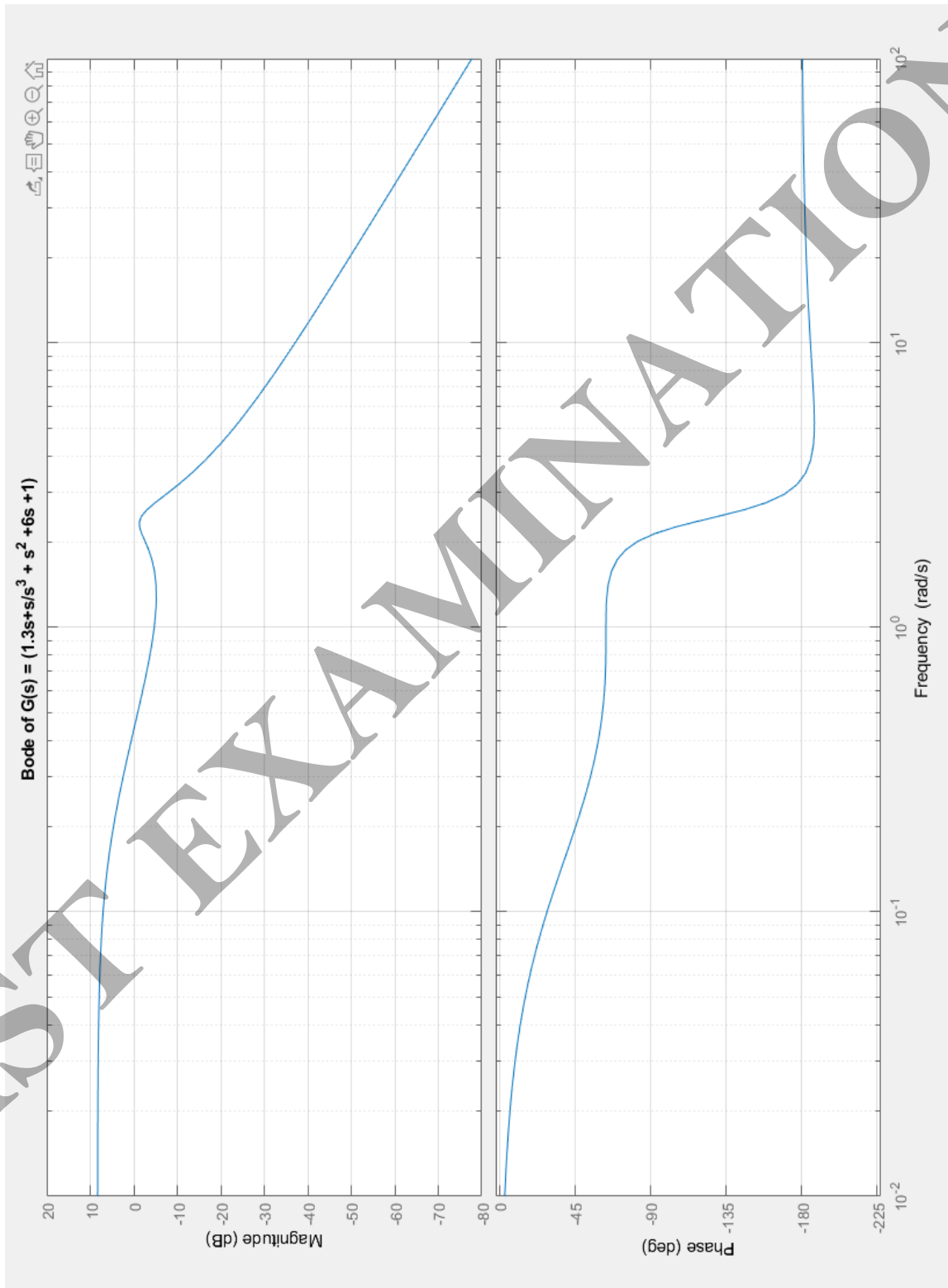


Figure 3(b)

Total: 25 marks  
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**Question 4**

- a) Steam at 7 bar, dryness fraction 0.9 expands reversibly at constant pressure until the temperature is 200 °c. Calculate the work input and heat supplied per unit mass of steam during the process.

**[15 Marks]**

- b) Steam at 0.05 bar, 100 °c is to be condensed completely by a reversible constant pressure process. Calculate the heat rejected per kilogramme of steam and the change of specific entropy.

**[10 Marks]****Total: 25 marks****Question 5**

- a) Derive the Darcy Weisbach Equation  $h_f = \frac{fLV^2}{2gD}$  for the loss of Head due to friction in a pipeline using the energy equation

$$\frac{P_1}{\rho g} + Z_1 + \frac{V_1^2}{2g} = \frac{P_2}{\rho g} + Z_2 + \frac{V_2^2}{2g} + HL$$

Where HL= the friction head loss  $h_f$ .**[17marks]**

- b) Oil with specific gravity of 0.85 with kinematic viscosity of  $6 \times 10^{-4} \text{ m}^2/\text{s}$  flows in a 15 cm pipe at a rate of  $0.020 \text{ m}^3/\text{s}$ . What is the head loss per 100 m length of pipe?

**[8 marks]****Total marks: 25 marks****Please turn the page...**

**Question 6**

a)

A Prototype gate valve, which will control the flow in a pipe system conveying paraffin, is to be studied in a model. The pressure drop  $\Delta P$  is expected to depend upon the gate opening  $h$ , the overall depth  $d$ , the velocity  $V$ , density  $\rho$  and viscosity  $\mu$ . Perform dimensional analysis to obtain the relevant non-dimensional groups.

**[15 marks]**

b)

A Carnot engine is used in a nuclear power plant. It receives 1500 Mw of power as a heat transfer from a source at 327 °C and rejects thermal waste to a nearby river at 27 °C. The river temperature rises by 3 K because of this power rejection by the plant,

Calculate:

- i) The mass flow rate of the river
- ii) The efficiency of the power plant

Take the value of specific heat capacity  $C_p=4.177\text{kJ/kg K}$

**[10 marks]**

**Total marks: 25 marks**

**END OF QUESTIONS**

**Formula sheet follows over the page...**

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PLEASE TURN THE PAGE FOR FORMULA SHEETS AND PROPERTY TABLES...

Formula sheet

**Blocks with feedback loop**

$$G(s) = \frac{Go(s)}{1 + Go(s)H(s)} \text{ (for a negative feedback)}$$

$$G(s) = \frac{Go(s)}{1 - Go(s)H(s)} \text{ (for a positive feedback)}$$

**Steady-State Errors**

$$e_{ss} = \lim_{s \rightarrow 0} [s \frac{1}{1 + G_o(s)} \theta_i(s)] \text{ (for the closed-loop system with a unity feedback)}$$

$$e_{ss} = \lim_{s \rightarrow 0} [s \frac{1}{1 + \frac{G_o(s)}{1 + G_o(s)[H(s) - 1]} } \theta_i(s)] \text{ (if the feedback } H(s) \neq 1)$$

$$e_{ss} = \frac{1}{1 + \lim_{z \rightarrow 1} G_o(z)} \text{ (if a digital system subjects to a unit step input)}$$

**Laplace Transforms**

A unit impulse function 1

A unit step function  $\frac{1}{s}$

A unit ramp function  $\frac{1}{s^2}$

**First order Systems**

$$G(s) = \frac{\theta_o}{\theta_i} = \frac{G_u(s)}{s\tau + 1}$$

$$\tau \left( \frac{d\theta_o}{dt} \right) + \theta_o = G_u \theta_i$$

$$\theta_o = G_u (1 - e^{-t/\tau}) \text{ (for a unit step input)}$$

$$\theta_o = A G_u (1 - e^{-t/\tau}) \text{ (for a step input with size } A)$$

$$\theta_o(t) = G_u \left( \frac{1}{\tau} \right) e^{-(t/\tau)} \text{ (for an impulse input)}$$

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### Second-order systems

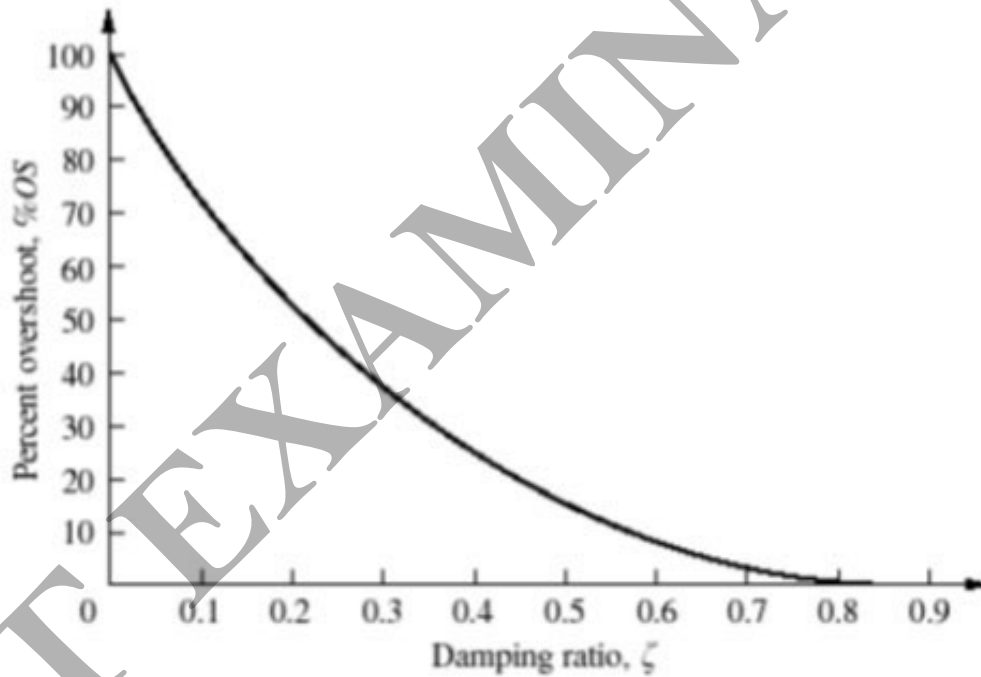
$$\frac{d^2\theta_o}{dt^2} + 2\zeta\omega_n \frac{d\theta_o}{dt} + \omega_n^2\theta_o = b_o\omega_n^2\theta_i$$

$$G(s) = \frac{\theta_o(s)}{\theta_i(s)} = \frac{b_o\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$\omega_{dt} = 1/2\pi \quad \omega_{dp} = \pi$$

$$\text{P.O.} = \exp\left(\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}\right) \times 100\%$$

$$t_s = \frac{4}{\zeta\omega_n} \quad \omega_d = \omega_n\sqrt{1-\zeta^2}$$



Controllability:  $R = [B \ AB \ A^2B \ \dots \ A^{(n-1)}B]$

Observability:

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## Laplace transform and Z transform table

Laplace Domain	Time Domain	Z Domain
1	$\delta(t)$ unit impulse	1
$\frac{1}{s}$	$u(t)$ unit step	$\frac{z}{z-1}$
$\frac{1}{s^2}$	$t$	$\frac{Tz}{(z-1)^2}$
$\frac{1}{s+a}$	$e^{-at}$	$\frac{z}{z-e^{-aT}}$
$\frac{1}{s(s+a)}$	$\frac{1}{a}(1-e^{-at})$	$\frac{z(1-e^{-aT})}{a(z-1)(z-e^{-aT})}$
$\frac{b-a}{(s+a)(s+b)}$	$e^{-at} - e^{-bt}$	$\frac{z(e^{-aT} - e^{-bT})}{a(z-e^{-aT})(z-e^{-bT})}$
$\frac{b}{(s+a)^2 + b^2}$	$e^{-at} \sin(bt)$	$\frac{ze^{-aT} \sin(bT)}{z^2 - 2ze^{-aT} \cos(bT) + e^{-2aT}}$
$\frac{s+a}{(s+a)^2 + b^2}$	$e^{-at} \cos(bt)$	$\frac{z^2 - ze^{-aT} \cos(bT)}{z^2 - 2ze^{-aT} \cos(bT) + e^{-2aT}}$

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### *Laplace Transforms of common functions*

<b>Functions</b>		
Unit pulse (Dirac delta distribution)	$\delta(t)$	$F(s) = 1$
Unit step function	$1(t)$	$F(s) = \frac{1}{s}$
Ramp function	$f(t) = at$	$F(s) = \frac{1}{s^2}$
Sine function	$f(t) = \sin at$	$F(s) = \frac{a}{s^2 + a^2}$
Cosine function	$f(t) = \cos at$	$F(s) = \frac{s}{s^2 + a^2}$
Exponential function	$f(t) = e^{at}$	$F(s) = \frac{1}{s - a}$
<b>Operations</b>		
Differentiation	$L(f'(t))$	$sF(s) - f(0)$
Integration	$L\left(\int f(t) dt\right)$	$\frac{1}{s} F(s)$
Time shift	$Lf(t - a)$	$e^{-as} F(s)$

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$$W = \frac{P_1 V_1 - P_2 V_2}{n-1} \quad W = P (v_2 - v_1)$$

$$W = PV \ln \left( \frac{V_2}{V_1} \right)$$

$$Q = C_d A \sqrt{2gh}$$

$$V_1 = C \sqrt{2g h_2 \left( \frac{\rho_{\text{gas}}}{\rho_{\text{liq}}} - 1 \right)}$$

$$\sum F = \frac{\Delta M}{\Delta t} = \Delta M$$

$$F = \rho QV$$

$$Re = VL \rho / \mu$$

$$dQ = du + dw$$

$$du = cu \, dT$$

$$dw = pdv$$

$$pv = mRT$$

$$h = hf + xhfg$$

$$s = sf + xsfg$$

$$v = x Vg$$

$$Q - w = \sum mh$$

$$F = \frac{2\pi L \mu}{L_1 \left( \frac{R_2}{R_1} \right)}$$

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$$S_g = C_{\mu} L_n \frac{T}{273} + \frac{h_g}{T_f}$$

$$S = C_{\mu} L_n \frac{T_f}{273} + \frac{hf_g}{T_f} + C_{\mu} L_n \frac{T}{T_f}$$

$$S_2 - S_1 = MC_p L_n \frac{T_2}{T_1} - MRL_n \frac{P_2}{P_1}$$

$$F_D = \frac{1}{2} CD \rho u^2 s$$

$$F_L = \frac{1}{2} C_L \rho u^2 s$$

$$S_p = \frac{d}{ds} (P + \rho g Z)$$

$$Q = \frac{\pi D^4 \Delta p}{128 \mu L}$$

$$h_f = \frac{64}{R} \left( \frac{L}{D} \right) \left( \frac{v^2}{2g} \right)$$

$$h_f = \frac{4fL v^2}{d2g}$$

$$f = \frac{16}{Re}$$

$$h_m = \frac{Kv^2}{2g}$$

$$h_m = \frac{k(V_1 - V_2)^2}{2g}$$

$$\zeta = \left( 1 - \frac{T_2}{T_1} \right)$$

$$S_{gen} = (S_2 - S_1) + \frac{Q}{T}$$

$$W = (U_1 - U_2) - T_0(S_1 - S_2) - T_0 S_{gen}$$

$$W_s = W - P_0(V_2 - V_1)$$

$$W_{rev} = (U_1 - U_2) - T_0(S_1 - S_2) + P_0(V_1 - V_2)$$

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$$\Phi = (U - U_0) - T(S - S_0) + P_0(V - V_0)$$

$$I = T_0 S_{gen}$$

$$V = r\omega$$

$$\lambda = \mu \frac{V}{t}$$

$$F = \frac{2\pi L \mu u}{L_n \left( \frac{R_2}{R_1} \right)}$$

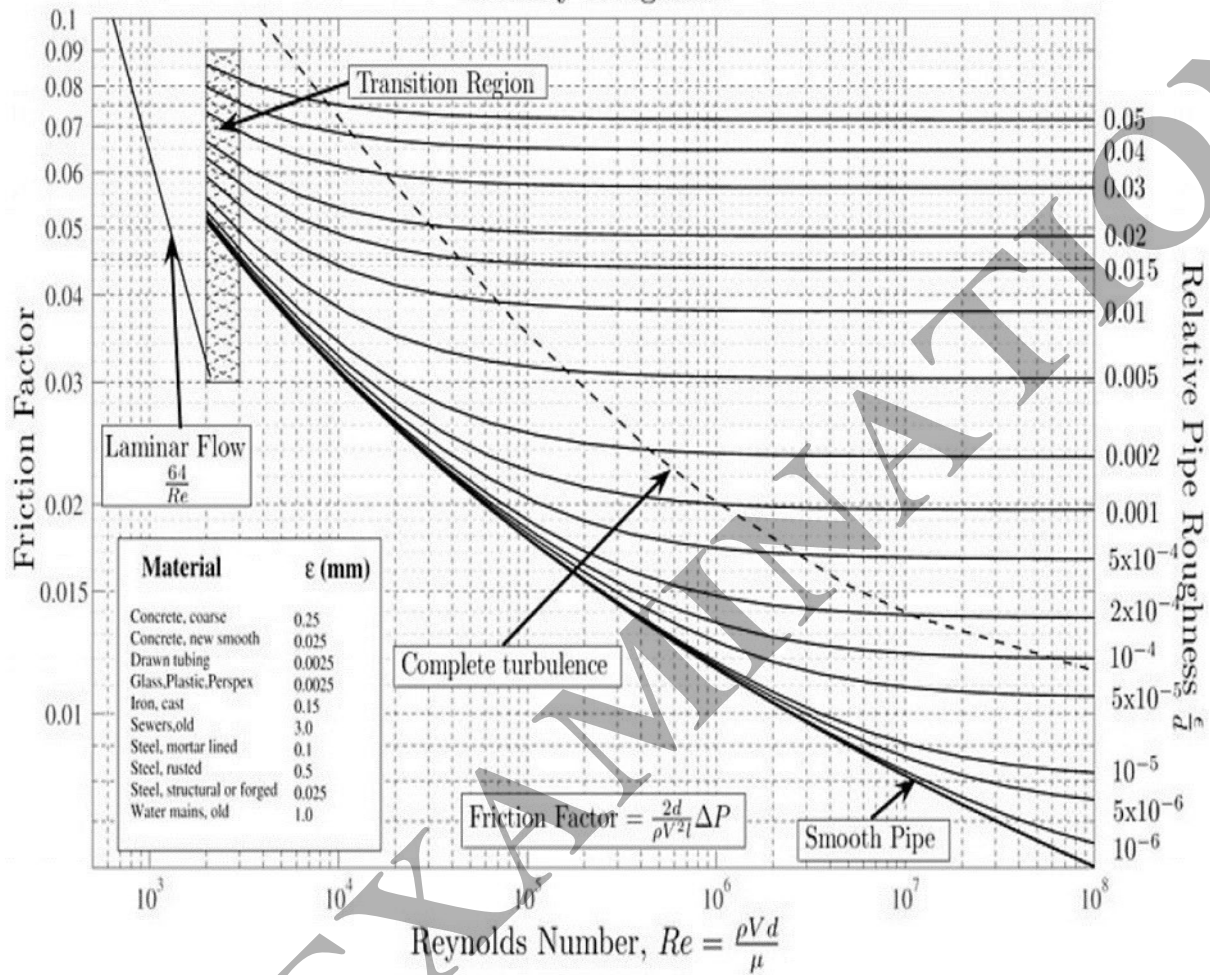
$$T = \frac{\pi^2 \mu N}{60t} (R_1^4 - R_2^4)$$

$$p = \frac{\rho g Q H}{1000}$$

PAST EXAMINATION

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Moody Diagram



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### DIMENSIONS FOR CERTAIN PHYSICAL QUANTITIES

Quantity	Symbol	Dimensions	Quantity	Symbol	Dimensions
Mass	m	M	Mass /Unit Area	$m/A^2$	$ML^{-2}$
Length	l	L	Mass moment	ml	ML
Time	t	T	Moment of Inertia	I	$ML^2$
Temperature	T	$\theta$	-	-	-
Velocity	u	$LT^{-1}$	Pressure /Stress	$p/\sigma$	$ML^{-1}T^{-2}$
Acceleration	a	$LT^{-2}$	Strain	$\tau$	$M^0L^0T^0$
Momentum/Impulse	mv	$MLT^{-1}$	Elastic Modulus	E	$ML^{-1}T^{-2}$
Force	F	$MLT^{-2}$	Flexural Rigidity	EI	$ML^3T^{-2}$
Energy - Work	W	$ML^2T^{-2}$	Shear Modulus	G	$ML^{-1}T^{-2}$
Power	P	$ML^2T^{-3}$	Torsional rigidity	GJ	$ML^3T^{-2}$
Moment of Force	M	$ML^2T^{-2}$	Stiffness	k	$MT^{-2}$
Angular momentum	-	$ML^2T^{-1}$	Angular stiffness	$T/\eta$	$ML^2T^{-2}$
Angle	$\eta$	$M^0L^0T^0$	Flexibility	$1/k$	$M^{-1}T^2$
Angular Velocity	$\omega$	$T^{-1}$	Vorticity	-	$T^{-1}$
Angular acceleration	$\alpha$	$T^{-2}$	Circulation	-	$L^2T^{-1}$
Area	A	$L^2$	Viscosity	$\mu$	$ML^{-1}T^{-1}$
Volume	V	$L^3$	Kinematic Viscosity	$\nu$	$L^2T^{-1}$
First Moment of Area	$Ar$	$L^3$	Diffusivity	-	$L^2T^{-1}$
Second Moment of Area	I	$L^4$	Friction coefficient	$f/\mu$	$M^0L^0T^0$
Density	$\rho$	$ML^{-3}$	Restitution coefficient	-	$M^0L^0T^0$
Specific heat-Constant Pressure	$C_p$	$L^2T^{-2}\theta^{-1}$	Specific heat-Constant volume	$C_v$	$L^2T^{-2}\theta^{-1}$

Note:  $a$  is identified as the local sonic velocity, with dimensions  $L \cdot T^{-1}$

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