[ENG17]

UNIVERSITY OF BOLTON

SCHOOL OF ENGINEERING

BENG (HONS) ELECTRICAL & ELECTRONICS ENGINEERING

SEMESTER ONE EXAMINATION 2021/2022

ENGINEERING ELECTROMAGNETISM

MODULE NO: EEE6012

Date: Friday 14th January 2022

Time: 10:00 – 12:00

INSTRUCTIONS TO CANDIDATES:

There are <u>SIX</u> questions.

Answer <u>ANY FOUR</u> questions.

All questions carry equal marks.

Marks for parts of questions are shown in brackets.

Electronic calculators may be used provided that data and program storage memory is cleared prior to the examination.

CANDIDATES REQUIRE:

Formula Sheet (attached).

Question 1

Q1. a) An electromagnetic wave is propagating in the y-direction in a lossy medium with attenuation constant $\alpha = 0.5 \frac{Np}{m}$. If the wave's electric-field amplitude is 100 V/m at y=0. How far can the wave travel before its amplitude will have been reduced to (i) 15 V/m , (ii) 1.5 V/m, (iii) $1\mu V/m$. **[5 marks]**

b) A series RLC circuit is connected to a voltage source given by $v_s(t) = 150\cos \omega t V$. Find (i) the phasor current I and (ii) the instantaneous current i(t) for R=400 Ω , L= 3 mH, C=20 n*F*, and $\omega = 10^5 rad/s$. **[8 marks]**

- c) Two points in a Cartesian coordinates are P1(1,2,3) and P2(-1,-2,3). Find
 - (i) the distance vector between P1 and P2.
 - (ii) the angle between vectors $\overrightarrow{OP1}$ and $\overrightarrow{OP2}$ using the cross product between them.
 - (iii) the angle between vector $\overrightarrow{OP2}$ and the y-axis.

[12 marks]

Total 25 marks

Question 2

- a) a) Transform vector $\mathbf{A} = \hat{\mathbf{x}} (x + y) + \hat{\mathbf{y}} (y x) + \hat{\mathbf{z}} z$ from Cartesian to Cylindrical coordinates. [6 marks]
- **b)** A scalar quantity of $V = rz^2 cos 2\phi$. Find its directional derivative along the direction $\mathbf{A} = \hat{\mathbf{r}} \mathbf{2} \hat{\mathbf{z}} \mathbf{3}$ and evaluate it at $(1, 0.5\pi, 2)$. [9 marks]
- c) Find the divergence and the curl of the given vector $A=e^{-7y}(\hat{x}\sin 3x+\hat{y}\cos 3x)$ at x=10 and y=1.0. [10 marks]

Total 25 marks

Question 3

a) A circular disk sitting at the x-y plane with z=0 is characterised by an azimuthally symmetric surface charge density that increases linearly with radius r from zero to 8 C/m² at r=4 cm. Find the total charge present on the disk surface.

[6 marks]

- b) Two point charges with q1=3X10⁻⁵ C and q2=-5X10⁻⁵ C are located in free space at points with Cartesian coordinates (1,3,-1) and (-3,1,-2) respectively . Find
 - i) the electric field **E** at (3,1,-2)

[7 marks]

ii) the force on a 7X10⁻⁵ C charge located at that point. All distances are in metres. [3 marks]

c) Derive a formula for the inductance of a cylindrical conductor due to (i) internal flux and (ii) external flux assuming the conductor is surrounded by air.

[9 marks] Total 25 marks

Question 4

- a) An Ethernet cable has L= 0.22 µHm⁻¹ and C = 86 pFm⁻¹. What is the wavelength at 10 MHz ? [6 marks]
- b) Assuming the loss resistance of a half-wave dipole antenna to be negligibly small and ignoring the reactance component of its antenna impedance, calculate the standing wave ratio on a 50-W transmission line connected to the dipole antenna. Note that a half wave dipole has a radiation resistance of 73 Ω . [6 marks]
- c) A transponder with a bandwidth of 400 MHz uses polarization diversity. If the bandwidth allocated to transmit a single telephone channel is 4 kHz, how many telephone channels can be carried by the transponder? [4 marks]
- d) A remote sensing satellite is in circular orbit around the earth at an altitude of 1,100 km above the earth's surface. What is its orbital period? Assume that the radius of the earth is 6,378 km. [9 marks]

Total 25 marks

Question 5

A source $[\tilde{V}_g = 100 \ge 0^\circ V, Z_g = R_g = 50 \Omega, f = 100 MHz]$ is connected to a lossless transmission line $[L = 0.25 \mu$ H/m, C=100pF/m, l=10m]. For loads of $Z_L = R_L = 100 \Omega$, determine the

a) reflection coefficient at the load	[6 marks]
b) standing wave ratio	[2 marks]
c) input impedance at the transmission line input terminals	[7 marks]
d) voltage along the transmission line for load of $Z_L = R_L = 100 \Omega$.	[10 marks]

Question 6

a) An antenna has a field pattern given by $E(\theta) = \cos\theta \cos 2\theta$ for $0^\circ \le \theta \le 90^\circ$. Calculate the:

i.	half-power beamwidth (HPBW)	[7 marks]
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- ii. beamwidth between first nulls (FNBW) [3 marks]
- b) A lossless resonant half-wavelength dipole antenna, with input impedance of 73 Ω , is connected to a transmission line whose characteristic impedance is 50 ohms. Assuming that the pattern of the antenna is given by approximately $U = B_0 \sin^3 \theta$. Determine the maximum dB gain of this antenna. [15 marks]

Total 25 marks

Total 25 marks

END OF QUESTIONS

Formula sheet follows over the page....

Formula sheet

These equations are given to save short-term memorisation of details of derived equations and are given without any explanation or definition of symbols; the student is expected to know the meanings and usage.

Time-domain sinusoidal functions z(t) and their cosinereference phasor-domain counterparts \tilde{Z} , where $z(t) = \Re e [\tilde{Z}e^{j\omega t}]$.

Z(t)		\widetilde{Z}
$A \cos \omega t$ $A \cos(\omega t + \phi_0)$ $A \cos(\omega t + \beta x + \phi_0)$ $A e^{-\alpha x} \cos(\omega t + \beta x + \phi_0)$ $A \sin \omega t$ $A \sin(\omega t + \phi_0)$	* * * * * * *	A $Ae^{j\phi_0}$ $Ae^{j(\beta x + \phi_0)}$ $Ae^{-\alpha x}e^{j(\beta x + \phi_0)}$ $Ae^{-j\pi/2}$ $Ae^{j(\phi_0 - \pi/2)}$
$\frac{d}{dt}(z(t))$	\Leftrightarrow	$j\omega\widetilde{Z}$
$\frac{d}{dt}[A\cos(\omega t + \phi_0)]$	\Leftrightarrow	$j\omega Ae^{j\phi_0}$
$\int z(t)dt$	\Leftrightarrow	$\frac{1}{j\omega}\widetilde{Z}$
$\int A\sin(\omega t + \phi_0) dt$	\Leftrightarrow	$\frac{1}{j\omega}Ae^{j(\phi_0-\pi/2)}$

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	Summary of vector relations.		
	Cartesian	Cylindrical	Spherical
	Coordinates	Coordinates	Coordinates
Coordinate variables	x, y, Z	r, ϕ, z	$R, heta, \phi$
Vector representation A =	$\hat{\mathbf{x}}A_x + \hat{\mathbf{y}}A_y + \hat{\mathbf{z}}A_z$	$\hat{\mathbf{r}}A_r + \hat{\mathbf{\phi}}A_\phi + \hat{\mathbf{z}}A_z$	$\hat{\mathbf{R}}A_R + \hat{\mathbf{\Theta}}A_\theta + \hat{\mathbf{\phi}}A_\phi$
Magnitude of A A =	$\sqrt[+]{A_x^2 + A_y^2 + A_z^2}$	$\sqrt[+]{A_r^2 + A_\phi^2 + A_z^2}$	$\sqrt[+]{A_R^2 + A_\theta^2 + A_\phi^2}$
Position vector $\overrightarrow{OP_1} =$	$\hat{\mathbf{x}}x_1 + \hat{\mathbf{y}}y_1 + \hat{\mathbf{z}}z_1,$	$\hat{\mathbf{r}}r_1 + \hat{\mathbf{z}}z_1,$	$\hat{\mathbf{R}}R_1$,
	for $P = (x_1, y_1, z_1)$	for $P = (r_1, \phi_1, z_1)$	for $P = (R_1, \theta_1, \phi_1)$
Base vectors properties	$\hat{\mathbf{x}} \cdot \hat{\mathbf{x}} = \hat{\mathbf{y}} \cdot \hat{\mathbf{y}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{z}} = 1$	$\hat{\mathbf{r}}\cdot\hat{\mathbf{r}}=\hat{\mathbf{\phi}}\cdot\hat{\mathbf{\phi}}=\hat{\mathbf{z}}\cdot\hat{\mathbf{z}}=1$	$\hat{\mathbf{R}} \cdot \hat{\mathbf{R}} = \hat{\mathbf{\theta}} \cdot \hat{\mathbf{\theta}} = \hat{\mathbf{\phi}} \cdot \hat{\mathbf{\phi}} = 1$
	$\hat{\mathbf{x}} \cdot \hat{\mathbf{y}} = \hat{\mathbf{y}} \cdot \hat{\mathbf{z}} = \hat{\mathbf{z}} \cdot \hat{\mathbf{x}} = 0$	$\hat{\mathbf{r}}\cdot\hat{\mathbf{\phi}}=\hat{\mathbf{\phi}}\cdot\hat{\mathbf{z}}=\hat{\mathbf{z}}\cdot\hat{\mathbf{r}}=0$	$\hat{\mathbf{R}}\cdot\hat{\mathbf{\theta}}=\hat{\mathbf{\theta}}\cdot\hat{\mathbf{\phi}}=\hat{\mathbf{\phi}}\cdot\hat{\mathbf{R}}=0$
	$\hat{\mathbf{x}} \times \hat{\mathbf{y}} = \hat{\mathbf{z}}$	$\hat{\mathbf{r}} \times \hat{\mathbf{\phi}} = \hat{\mathbf{z}}$	$\hat{\mathbf{R}} \times \hat{\mathbf{\Theta}} = \hat{\mathbf{\phi}}$
	$\hat{\mathbf{y}} \times \hat{\mathbf{z}} = \hat{\mathbf{x}}$	$\hat{\mathbf{\phi}} \mathbf{x} \hat{\mathbf{z}} = \hat{\mathbf{r}}$	$\hat{\mathbf{\Theta}} imes \hat{\mathbf{\varphi}} = \hat{\mathbf{R}}$
	$\hat{z} \times \hat{x} = \hat{y}$	$\hat{\mathbf{z}} \times \hat{\mathbf{r}} = \hat{\mathbf{\phi}}$	$\hat{\mathbf{\phi}} imes \hat{\mathbf{R}} = \hat{\mathbf{\Theta}}$
Dot product $\mathbf{A} \cdot \mathbf{B} =$	$A_X B_X + A_Y B_Y + A_Z B_Z$	$A_r B_r + A_\phi B_\phi + A_Z B_Z$	$A_R B_R + A_\theta B_\theta + A_\phi B_\phi$
Cross product A × B =	$\begin{vmatrix} \hat{\mathbf{x}} & \hat{\mathbf{y}} & \hat{\mathbf{z}} \\ A_x & A_y & A_z \\ B_x & B_y & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{\mathbf{r}} & \hat{\boldsymbol{\phi}} & \hat{\boldsymbol{z}} \\ A_r & A_{\phi} & A_z \\ B_r & B_{\phi} & B_z \end{vmatrix}$	$\begin{vmatrix} \hat{\mathbf{R}} & \hat{\mathbf{\Theta}} & \hat{\mathbf{\varphi}} \\ A_R & A_\theta & A_\phi \\ B_R & B_\theta & B_\phi \end{vmatrix}$
Differential length $d\mathbf{l} =$	$\hat{\mathbf{x}} dx + \hat{\mathbf{y}} dy + \hat{\mathbf{z}} dz$	$\hat{\mathbf{r}} dr + \hat{\mathbf{\phi}} r d\phi + \hat{\mathbf{z}} dz$	$\hat{\mathbf{R}} dR + \hat{\mathbf{\theta}} R d\theta + \hat{\mathbf{\phi}} R \sin \theta d\phi$
Differential surface areas	$ds_x = \hat{x} dy dz$ $ds_y = \hat{y} dx dz$ $ds_z = \hat{z} dx dy$	$ds_r = \hat{\mathbf{r}}r \ d\phi \ dz$ $ds_\phi = \hat{\mathbf{\phi}} \ dr \ dz$ $ds_z = \hat{\mathbf{z}}r \ dr \ d\phi$	$ds_{R} = \hat{\mathbf{R}}R^{2}\sin\theta \ d\theta \ d\phi$ $ds_{\theta} = \hat{\mathbf{\theta}}R\sin\theta \ dR \ d\phi$ $ds_{\phi} = \hat{\mathbf{\varphi}}R \ dR \ d\theta$
Differential volume $dV =$	dx dy dz	r dr dø dz	$R^2\sin\theta \ dR \ d\theta \ d\phi$

Transformation	Coordinate Variables	Unit Vectors	Vector Components
Cartesian to cylindrical	$r = \sqrt[+]{x^2 + y^2}$ $\phi = \tan^{-1}(y/x)$ z = z	$\hat{\mathbf{r}} = \hat{\mathbf{x}}\cos\phi + \hat{\mathbf{y}}\sin\phi$ $\hat{\mathbf{\phi}} = -\hat{\mathbf{x}}\sin\phi + \hat{\mathbf{y}}\cos\phi$ $\hat{\mathbf{z}} = \hat{\mathbf{z}}$	$A_r = A_x \cos \phi + A_y \sin \phi$ $A_\phi = -A_x \sin \phi + A_y \cos \phi$ $A_z = A_z$
Cylindrical to Cartesian	$x = r \cos \phi$ $y = r \sin \phi$ z = z	$\hat{\mathbf{x}} = \hat{\mathbf{r}}\cos\phi - \hat{\mathbf{\phi}}\sin\phi$ $\hat{\mathbf{y}} = \hat{\mathbf{r}}\sin\phi + \hat{\mathbf{\phi}}\cos\phi$ $\hat{\mathbf{z}} = \hat{\mathbf{z}}$	$A_x = A_r \cos \phi - A_\phi \sin \phi$ $A_y = A_r \sin \phi + A_\phi \cos \phi$ $A_z = A_z$
Cartesian to spherical	$R = \sqrt[+]{x^2 + y^2 + z^2}$ $\theta = \tan^{-1}[\sqrt[+]{x^2 + y^2}/z]$ $\phi = \tan^{-1}(y/x)$	$\hat{\mathbf{R}} = \hat{\mathbf{x}} \sin \theta \cos \phi$ + $\hat{\mathbf{y}} \sin \theta \sin \phi + \hat{\mathbf{z}} \cos \theta$ $\hat{\mathbf{\theta}} = \hat{\mathbf{x}} \cos \theta \cos \phi$ + $\hat{\mathbf{y}} \cos \theta \sin \phi - \hat{\mathbf{z}} \sin \theta$ $\hat{\mathbf{\phi}} = -\hat{\mathbf{x}} \sin \phi + \hat{\mathbf{y}} \cos \phi$	$A_{R} = A_{x} \sin \theta \cos \phi$ + $A_{y} \sin \theta \sin \phi + A_{z} \cos \theta$ $A_{\theta} = A_{x} \cos \theta \cos \phi$ + $A_{y} \cos \theta \sin \phi - A_{z} \sin \theta$ $A_{\phi} = -A_{x} \sin \phi + A_{y} \cos \phi$
Spherical to Cartesian	$x = R \sin \theta \cos \phi$ $y = R \sin \theta \sin \phi$ $z = R \cos \theta$	$\hat{\mathbf{x}} = \hat{\mathbf{R}} \sin \theta \cos \phi$ $+ \hat{\mathbf{\theta}} \cos \theta \cos \phi - \hat{\mathbf{\phi}} \sin \phi$ $\hat{\mathbf{y}} = \hat{\mathbf{R}} \sin \theta \sin \phi$ $+ \hat{\mathbf{\theta}} \cos \theta \sin \phi + \hat{\mathbf{\phi}} \cos \phi$ $\hat{\mathbf{z}} = \hat{\mathbf{R}} \cos \theta - \hat{\mathbf{\theta}} \sin \theta$	$A_x = A_R \sin \theta \cos \phi$ + $A_\theta \cos \theta \cos \phi - A_\phi \sin \phi$ $A_y = A_R \sin \theta \sin \phi$ + $A_\theta \cos \theta \sin \phi + A_\phi \cos \phi$ $A_z = A_R \cos \theta - A_\theta \sin \theta$
Cylindrical to spherical	$R = \sqrt[+]{r^2 + z^2}$ $\theta = \tan^{-1}(r/z)$ $\phi = \phi$	$\hat{\mathbf{R}} = \hat{\mathbf{r}} \sin \theta + \hat{\mathbf{z}} \cos \theta$ $\hat{\mathbf{\theta}} = \hat{\mathbf{r}} \cos \theta - \hat{\mathbf{z}} \sin \theta$ $\hat{\mathbf{\phi}} = \hat{\mathbf{\phi}}$	$A_R = A_r \sin \theta + A_z \cos \theta$ $A_\theta = A_r \cos \theta - A_z \sin \theta$ $A_\phi = A_\phi$
Spherical to cylindrical	$r = R \sin \theta$ $\phi = \phi$ $z = R \cos \theta$	$\hat{\mathbf{r}} = \hat{\mathbf{R}}\sin\theta + \hat{\mathbf{\theta}}\cos\theta$ $\hat{\mathbf{\phi}} = \hat{\mathbf{\phi}}$ $\hat{\mathbf{z}} = \hat{\mathbf{R}}\cos\theta - \hat{\mathbf{\theta}}\sin\theta$	$A_r = A_R \sin \theta + A_\theta \cos \theta$ $A_\phi = A_\phi$ $A_z = A_R \cos \theta - A_\theta \sin \theta$

Coordinate transformation relations.

$$\begin{split} \mathbf{ELECTROSTATICS:} \\ \mathbf{F}_{12} &= \frac{Q_1 Q_2}{4\pi\varepsilon_0 R^2} \mathbf{a}_{R_{12}} \ , \ \mathbf{F} = \frac{Q}{4\pi\varepsilon_0} \sum_{k=1}^N \frac{Q_k (\mathbf{r} - \mathbf{r}_k)}{|\mathbf{r} - \mathbf{r}_k|^3} \ , \ \mathbf{E} = \frac{\mathbf{F}}{Q} \ , \ \mathbf{E} = \int \frac{\rho_L dl}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_S dS}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_L dl}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_S dS}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_L dl}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_L dl}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_L dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_L dl}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \int \frac{\rho_V dv}{4\pi\varepsilon_0 R^2} \mathbf{a}_R \ , \ \mathbf{E} = \frac{\rho_V dv}{R} \ , \ \mathbf{E} \ , \ \mathbf$$

$$\begin{split} \mathbf{MAGNETOSTATICS:} \\ \mathbf{H} &= \int_{L} \frac{Id\mathbf{I} \times \mathbf{a}_{R}}{4\pi R^{2}}, \ \mathbf{H} = \int_{S} \frac{\mathbf{K}dS \times \mathbf{a}_{R}}{4\pi R^{2}}, \ \mathbf{H} = \int_{V} \frac{Jdv \times \mathbf{a}_{R}}{4\pi R^{2}}, \ \mathbf{H} = \frac{I}{4\pi\rho} (\cos\alpha_{2} - \cos\alpha_{1})\mathbf{a}_{\phi}, \ \mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_{\phi}, \ \mathbf{a}_{\phi} = \mathbf{a}_{\ell} \times \mathbf{a}_{\rho}, \\ \oint \mathbf{H} \cdot d\mathbf{I} = I_{enc}, \ \nabla \times \mathbf{H} = \mathbf{J}, \ \mathbf{H} = \frac{I}{2\pi\rho} \mathbf{a}_{\phi}, \ \mathbf{H} = \frac{1}{2} \mathbf{K} \times \mathbf{a}_{n}, \ \mathbf{B} = \mu \mathbf{H}, \ \Psi = \int_{S} \mathbf{B} \cdot d\mathbf{S}, \ \oint \mathbf{B} \cdot d\mathbf{S} = 0, \ \nabla \cdot \mathbf{B} = 0, \ \mathbf{H} = -\nabla \mathbf{V}_{m}, \\ \mathbf{B} = \nabla \times \mathbf{A}, \ \mathbf{A} = \int_{L} \frac{\mu_{0} I d\mathbf{I}}{4\pi R}, \ \mathbf{A} = \int_{S} \frac{\mu_{0} \mathbf{K} dS}{4\pi R}, \ \mathbf{A} = \int_{v} \frac{\mu_{0} \mathbf{J} dv}{4\pi R}, \ \mathbf{H} = \oint_{L} \mathbf{A} \cdot d\mathbf{I}, \ \mathbf{F} = \mathcal{Q}(\mathbf{E} + \mathbf{u} \times \mathbf{B}), \ d\mathbf{F} = Id\mathbf{I} \times \mathbf{B}, \ \mathbf{B}_{1n} = \mathbf{B}_{2n}, \\ (\mathbf{H}_{1} - \mathbf{H}_{2}) \times \mathbf{a}_{n12} = \mathbf{K}, \ \mathbf{H}_{1t} = \mathbf{H}_{2t}, \ \frac{\tan\theta_{1}}{\tan\theta_{2}} = \frac{\mu_{1}}{\mu_{2}}, \ L = \frac{\lambda}{I} = \frac{N\psi}{I}, \ M_{12} = \frac{\lambda_{12}}{I_{2}} = \frac{N_{1}\psi_{12}}{I_{2}}, \ W_{m} = \frac{1}{2}\int \mathbf{B} \cdot \mathbf{H} dv = \frac{1}{2}\int \mu H^{2} dv \end{split}$$

WAVES AND APPLICATIONS:

$$\begin{aligned} \mathbf{V}_{enf} &= -\frac{d\psi}{dt} \quad , \mathbf{V}_{enf} = \oint_{L} \mathbf{E} \cdot d\mathbf{I} = -\int_{S} \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S} \quad , \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \quad , \mathbf{V}_{enf} = \oint_{L} \mathbf{E}_{m} \cdot d\mathbf{I} = \oint_{L} (\mathbf{u} \times \mathbf{B}) \cdot d\mathbf{I} \\ \mathbf{V}_{enf} &= \oint_{L} \mathbf{E} \cdot d\mathbf{I} = -\int_{S} \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S} + \oint_{L} (\mathbf{u} \times \mathbf{B}) \cdot d\mathbf{I} \quad , \mathbf{J}_{d} = \frac{\partial \mathbf{D}}{dt} \quad , \nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{dt} \quad , \beta = \frac{2\pi}{\lambda} , \gamma = \alpha + j\beta \\ \alpha &= o\sqrt{\frac{\mu\varepsilon}{2}} \left[\sqrt{1 + \left[\frac{\sigma}{\varpi\varepsilon}\right]^{2} - 1} \right], \quad \beta = o\sqrt{\frac{\mu\varepsilon}{2}} \left[\sqrt{1 + \left[\frac{\sigma}{\varpi\varepsilon}\right]^{2} + 1} \right], \quad \mathbf{E}(z, t) = E_{0}e^{-\alpha z} \cos(\omega t - \beta z)\mathbf{a}_{x} \\ |\underline{\eta}| &= \frac{\sqrt{\mu/\varepsilon}}{\left[1 + \left(\frac{\sigma}{\varpi\varepsilon}\right)^{2} \right]^{V_{4}}, \quad \tan 2\theta_{\eta} = \frac{\sigma}{\omega\varepsilon}, \quad \mathbf{H} = \frac{E_{0}}{|\underline{\eta}|}e^{-\alpha z} \cos(\omega t - \beta z - \theta_{\eta})\mathbf{a}_{y}, \quad \tan \theta = \frac{\sigma}{\omega\varepsilon}, \quad \mathbf{a}_{E} \times \mathbf{a}_{H} = \mathbf{a}_{k} \\ \eta_{0} &= \sqrt{\frac{\mu_{0}}{\varepsilon_{0}}} = 120\pi \approx 377\Omega, \quad p(t) = \mathbf{E} \times \mathbf{H}, \quad p_{ave}(z) = \frac{1}{2} \operatorname{Re}(\mathbf{E}_{z} \times \mathbf{H}^{*}z), \quad p_{ave}(z) = \frac{E_{0}^{2}}{2|\underline{\eta}|}e^{-2\alpha z} \cos\theta_{\eta}\mathbf{a}_{z}, \quad P_{ave} = \int_{S} p_{ave} \cdot d\mathbf{S}, \\ \Gamma &= \frac{E_{ro}}{E_{io}} = \frac{\eta_{2} - \eta_{1}}{\eta_{2} + \eta_{1}}, \quad \tau = \frac{E_{io}}{E_{io}} = \frac{2\eta_{2}}{\eta_{2} + \eta_{1}}, \quad s = \frac{|\mathbf{E}_{1}|_{\max}}{|\mathbf{E}_{1}|_{\min}} = |\mathbf{H}_{1}|_{\min}} = \frac{1 + |\Gamma|}{1 - |\Gamma|}, \quad k_{i} \sin\theta_{i} = k_{i} \sin\theta_{i}, \\ \Gamma_{1} &= \frac{E_{ro}}{E_{io}} = \frac{\eta_{2} \cos\theta_{i} - \eta_{1} \cos\theta_{i}}{\eta_{2} \cos\theta_{i} + \eta_{1} \cos\theta_{i}}, \quad \tau_{1} = \frac{E_{io}}{E_{io}} = \frac{2\eta_{2} \cos\theta_{i}}{\eta_{2} \cos\theta_{i} + \eta_{1} \cos\theta_{i}}, \quad s n^{2} \theta_{B} = \frac{1 - \mu_{2} \varepsilon_{1}/\mu_{1}\varepsilon_{2}}{1 - (\omega_{1}/\varepsilon_{2})^{2}}, \\ \Gamma_{1} &= \frac{E_{ro}}{E_{io}} = \frac{\eta_{2} \cos\theta_{i} - \eta_{1} \cos\theta_{i}}{\eta_{2} \cos\theta_{i} + \eta_{1} \cos\theta_{i}}, \quad s n^{2} \theta_{B} = \frac{1 - \mu_{1}\varepsilon_{2}/\mu_{2}\varepsilon_{1}}{1 - (\mu_{1}/\mu_{2})^{2}} \\ \mathbf{\omega} = \mathbf{\beta} \mathbf{C} \\ S &= \frac{|V_{max}|}{|V_{min}|} = \frac{1 + |\Gamma|}{1 - |\Gamma|} \end{aligned}$$

Antenna and Radar formula

<u>Dipole</u> Solid angle:

$$\Omega_{\rm p} = \iint_{4\pi} F(heta, \phi) \ d\Omega$$

Directivity:

$$D = \frac{4\pi}{\Omega_{\rm p}}$$
 $D = \frac{4\pi A_{\rm e}}{\lambda^2}$

Shorted dipoleHertzian
monopole
$$S_0 = \frac{15\pi I_0^2}{R^2} \left(\frac{l}{\lambda}\right)^2$$
 $R_{rad} = 80\pi^2 \left[\frac{dl}{\lambda}\right]^2$ $R_{rad} = 80\pi^2 \left(\frac{l}{\lambda}\right)^2$ $R_{rad} = \frac{1}{2}I_o^2 R_{rad}$

. . .

Half -wave dipole

$$\begin{split} \widetilde{E}_{\theta} &= j \ 60 I_0 \left\{ \frac{\cos[(\pi/2)\cos\theta]}{\sin\theta} \right\} \left(\frac{e^{-jkR}}{R} \right), \\ \widetilde{H}_{\phi} &= \frac{\widetilde{E}_{\theta}}{\eta_0} \ . \\ |E_{\phi s}| &= \frac{\eta_0 I_0 \cos\left(\frac{\pi}{2}\cos\theta\right)}{2\pi r \sin\theta} \\ |H_{\phi s}| &= \frac{I_0 \cos\left(\frac{\pi}{2}\cos\theta\right)}{2\pi r \sin\theta} \end{split}$$

For Transmission line

	Propagation Constant $\gamma = \alpha + j\beta$	Phase Velocity u _p	Characteristic Impedance Z ₀
General case	$\gamma = \sqrt{(R' + j\omega L')(G' + j\omega C')}$	$u_{\rm p} = \omega/\beta$	$Z_0 = \sqrt{\frac{(R' + j\omega L')}{(G' + j\omega C')}}$
Lossless (R' = G' = 0)	$\alpha = 0, \ \beta = \omega \sqrt{\varepsilon_{\rm r}}/c$	$u_{\rm p} = c/\sqrt{\varepsilon_{\rm r}}$	$Z_0 = \sqrt{L'/C'}$
Lossless coaxial	$\alpha = 0, \ \beta = \omega \sqrt{\varepsilon_{\rm r}}/c$	$u_{\rm p} = c/\sqrt{\varepsilon_{\rm r}}$	$Z_0 = \left(\frac{60}{\sqrt{\varepsilon_{\rm r}}} \right) \ln(b/a)$
Lossless two-wire	$\alpha = 0, \ \beta = \omega \sqrt{\varepsilon_{\rm r}}/c$	$u_{\rm p} = c/\sqrt{\varepsilon_{\rm r}}$	$Z_0 = (120/\sqrt{\varepsilon_{\mathbf{r}}})$ $\cdot \ln[(D/d) + \sqrt{(D/d)^2 - 1}]$
			$Z_0 \simeq \left(\frac{120}{\sqrt{\varepsilon_{\rm r}}}\right) \ln(2D/d),$ if $D \gg d$
Lossless parallel-plate	$\alpha = 0, \ \beta = \omega \sqrt{\varepsilon_{\rm r}}/c$	$u_{\rm p} = c/\sqrt{\varepsilon_{\rm r}}$	$Z_0 = \left(120\pi/\sqrt{\varepsilon_{\rm r}}\right)(h/w)$
Notes: (1) $\mu = \mu$ insulating materia d = wire diamete h = separation bei	t_{0} , $\varepsilon = \varepsilon_{\rm r}\varepsilon_{0}$, $c = 1/\sqrt{\mu_{0}\varepsilon_{0}}$, and $\sqrt{1}$. (2) For coaxial line, <i>a</i> and <i>b</i> are r and <i>D</i> = separation between wire tween the plates	$\sqrt{\mu_0/\varepsilon_0} \simeq (120\pi)$ radii of inner a centers. (4) Fo	r) Ω, where ε_r is the relative permittivity of nd outer conductors. (3) For two-wire line, r parallel-plate line, $w =$ width of plate and

Distortionless line

$$\gamma = \sqrt{RG} + j \omega \sqrt{LC}$$

$$\frac{R}{L} = \frac{G}{C} \quad Z_o = \sqrt{\frac{L}{C}}$$

Open-circuited line

$$\widetilde{V}_{oc}(d) = V_0^+ [e^{j\beta d} + e^{-j\beta d}] = 2V_0^+ \cos\beta d,$$

$$\widetilde{I}_{oc}(d) = \frac{V_0^+}{Z_0} [e^{j\beta d} - e^{-j\beta d}] = \frac{2jV_0^+}{Z_0} \sin\beta d,$$

$$Z_{\rm in}^{\rm oc} = \frac{\widetilde{V}_{\rm oc}(l)}{\widetilde{I}_{\rm oc}(l)} = -jZ_0 \cot\beta l.$$

Short-circuited line

$$\begin{aligned} \widetilde{V}_{\rm sc}(d) &= V_0^+ [e^{j\beta d} - e^{-j\beta d}] = 2jV_0^+ \sin\beta d, \\ \widetilde{I}_{\rm sc}(d) &= \frac{V_0^+}{Z_0} [e^{j\beta d} + e^{-j\beta d}] = \frac{2V_0^+}{Z_0} \cos\beta d, \\ Z_{\rm sc}(d) &= \frac{\widetilde{V}_{\rm sc}(d)}{\widetilde{I}_{\rm sc}(d)} = jZ_0 \tan\beta d. \end{aligned}$$

 $j\omega L_{\text{eq}} = jZ_0 \tan\beta l, \quad \text{if } \tan\beta l \ge 0$

$$\frac{1}{j\omega C_{\rm eq}} = jZ_0 \tan\beta l, \qquad \text{if } \tan\beta l \le 0$$

$$Z_{\rm in} = Z_{\rm o} \left[\frac{Z_L + jZ_{\rm o} \tan \beta \ell}{Z_{\rm o} + jZ_L \tan \beta \ell} \right]$$
$$Z_{\rm in} = Z_{\rm o} \left[\frac{Z_L + Z_{\rm o} \tanh \gamma \ell}{Z_{\rm o} + Z_L \tanh \gamma \ell} \right]$$
$$V_{\rm o} = \frac{Z_{\rm in}}{Z_{\rm in} + Z_g} V_g \quad I_{\rm o} = \frac{V_g}{Z_{\rm in} + Z_g}$$
$$V_g = V_L e^{j\beta \ell}$$

For a bistatic radar (one in which the transmitting and receiving antennas are separated), the power received is given by

$$P_r = \frac{G_{dt}G_{dr}}{4\pi} \left[\frac{\lambda}{4\pi r_1 r_2}\right]^2 \sigma P_{\rm rad}$$

For a monostatic radar, $r_1 = r_2 = r$ and $G_{dt} = G_{dr}$.

$$P_{\rm rec} = P_{\rm t} G_{\rm t} G_{\rm r} \left(\frac{\lambda}{4\pi R}\right)^2$$

END OF PAPER