## UNIVERSITY OF BOLTON

## SCHOOL OF ENGINEERING

# BENG (HONS) ELECTRICAL \& ELECTRONICS ENGINEERING <br> <br> SEMESTER ONE EXAMINATION 2021/2022 <br> <br> SEMESTER ONE EXAMINATION 2021/2022 <br> INTERMEDIATE ELECTRICAL PRINCIPLES \& ENABLING POWER ELECTRONICS 

## MODULE NO: EEE5013

Date: Monday $10^{\text {th }}$ January 2022

INSTRUCTIONS TO CANDIDATES:

Time: 10:00-12:30

There are SIX questions.
Answer ANY FOUR questions.
All questions carry equal marks.

Marks for parts of questions are shown in brackets.

Electronic calculators may be used provided that data and program storage memory is cleared prior to the examination.

CANDIDATES REQUIRE:
Formula Sheet (attached from page 8).

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## Question 1

a) Sketch an equivalent circuit of an ideal operational amplifier.
[7 marks]
b) Using Figure Q1, derive an expression for the output $V_{o}$ of the following circuit in terms of the input voltages $V_{1}$ and $V_{2}$.


Figure Q1
c) Also, determine the output voltage if $V_{1}=1 \mathrm{~V}$ and $V_{2}=0.5 \mathrm{~V}$.
d) A silicon transistor having a TJmax rating of $180^{\circ} \mathrm{C}$ will dissipate 20 W when its case temperature is $90^{\circ} \mathrm{C}$, calculate its thermal resistance.

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## Question 2

a) Differentiate between gauge pressure and absolute pressure.
[4 marks]
b) Water flows from $A$ to $D$ and $E$ through the series pipeline shown in Figure Q2. Given the pipe diameters, velocities, and flow rates below, complete the tabular data for this system.
[21 marks]


Figure Q2
Pipe $\quad$ Diameter $(\mathrm{mm}) \quad$ Flow rate $\left(\mathrm{m}^{3} \mathrm{~s}^{-1}\right) \quad$ Velocity $\left(\mathrm{m} \mathrm{s}^{-1}\right)$

| AB | $d_{1}=50$ | $Q_{1}=?$ | $\bar{v}_{1}=?$ |
| :--- | :--- | :--- | :--- |
| BC | $d_{2}=75$ | $Q_{2}=?$ | $\bar{v}_{2}=2.0$ |
| CD | $d_{3}=?$ | $Q_{3}=2 Q_{4}$ | $\bar{v}_{3}=1.5$ |
| DE | $d_{4}=30$ | $Q_{4}=0.5 Q_{3}$ | $\bar{v}_{4}=?$ |

Note that area can be determined as $\pi d^{2} / 4$.

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## Question 3

(a) A half-wave rectifier circuit is used to charge a 150 V battery as shown in figure Q3a below. Calculate [10 marks] and plot the current i [ 5 marks] along with $\mathrm{v}_{\mathrm{s}}$ if $V_{s}=120 \mathrm{~V}, \mathrm{f}=60 \mathrm{~Hz}$, and $\mathrm{L}=10 \mathrm{mH}$.


Figure Q3a
(b) A DC-DC buck converter has the following specifications:

Input voltage=110 V., maximum inductor current=300 A., Minimum inductor
current=140 A., ToN= 15 msec ., Toff= 12 msec . , RLoad=60 Ohms, Calculate:
i. Chopping frequency
ii. Duty cycle
iii. Output voltage
iv. The value of the inductor's inductance
v. The capacitor's capacitance for 1.6 V ripple when the peak output voltage reaches 62 V .
[1 marks]
[1 marks]
[2 marks]
[2 marks]

Total 25 marks

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## Question 4

(a) Draw a circuit diagram for a boost converter [4 marks], explain its operation [6 marks] and derive an expression for $\frac{V_{\text {out }}}{V_{\text {in }}}$ defining all parameters used in this circuit [2 marks].
[12 marks]
(b) Enumerate the basic grounding system then explain what is meant by static grounding.
(c) For a single-phase inductive load (with parallel resistance and inductance).
i. Prove that the active power is always positive, has an average value of $\frac{V . I}{2} \cos \theta$ and zero average reactive power both pulsating at double supply frequency $(2 \omega)$ where V and I are the peak values of the voltage and current and $\theta$ is the power factor angle of the load.
[5 marks]
ii. Draw the relevant waveforms for $v, i$, and $p$.
[4 marks]

Total 25 marks

PLEASE TURN THE PAGE....

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## Question 5

(a) Calculate the line voltages and the line currents of a $\mathrm{Y}-\mathrm{Y}$ source-load Connection. Given: $\mathrm{V}_{\mathrm{an}}=120 \angle 60^{\circ} \mathrm{V}$. The system is balanced three-phase system. The system impedances per phase are given as follows:
$Z_{\text {source }}=0.4+j 0.3 \Omega, Z_{\text {line }}=0.6+j 0.7 \Omega, Z_{\text {load }}=24+j 19 \Omega$.
(b) Assume a delta-connected load, with each leg $Z=100<80^{\circ} \Omega$, is supplied from a 3-phase supply with voltage of 13.8 kV (L-L) source. Find:
i. The complex power of the source and load.
ii. The load power factor, active power and reactive power.
[3 marks]
iii. The value of a shunt capacitor that brings the power factor of the load to unity. Assume system frequency is 50 Hz .

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## Question 6

a) A 3-phase, $50 \mathrm{~Hz}, 215 \mathrm{kV}$ power line is delivering load of 125 MW at 0.8 power factor lagging and has an impedance per phase of $186.78 \angle 79.46^{\circ} \Omega$. find:
(i) The value of a series capacitance that compensates $70 \%$ of its inductive reactance.
(ii) The new value of its receiving end voltage assuming its sending end voltage remains constant.
[10 marks]
b) (i). Prove mathematically that line to line voltage of a star-connected source is square root of three multiplied by its phase voltage and leads it by 30 degrees.
(ii). Prove mathematically that line current of a delta-connected load is square root of three multiplied by its phase current and lags it by 30 degrees.
[5 marks]

## Total 25 marks

## END OF QUESTIONS

Formula Sheet follows over the page....

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## Formula sheet

These equations are given to save short-term memorisation of details of derived equations and are given without any explanation or definition of symbols; the student is expected to know the meanings and usage.

Converters:

$$
\begin{aligned}
& \% \mathrm{THD}_{i}=100 \times \frac{I_{\mathrm{dis}}}{I_{s 1}} \\
& =100 \times \frac{\sqrt{I_{s}^{2}-I_{s 1}^{2}}}{I_{s 1}} \\
& =100 \times \sqrt{\sum_{h \neq 1}\left(\frac{I_{s h}}{I_{s 1}}\right)^{2}} \\
& \mathrm{PF}=\frac{V_{s} I_{s 1} \cos \phi_{1}}{V_{s} I_{s}}=\frac{I_{s 1}}{I_{s}} \cos \phi_{1} \\
& \text { DPF }=\cos \phi_{1} \\
& \mathrm{PF}=\frac{I_{s 1}}{I_{s}} \mathrm{DPF} \\
& \mathrm{PF}=\frac{1}{\sqrt{1+\mathrm{THD}_{i}^{2}}} \mathrm{DPF} \\
& A_{u}=\sqrt{2} V_{s}(1-\cos u)=\omega L_{s} I_{d} \\
& \cos u=1-\frac{\omega L_{s} I_{d}}{\sqrt{2} V_{s}} \\
& V_{d}=0.45 V_{s}-\frac{\text { area } A_{u}}{2 \pi}=0.45 V_{s}-\frac{\omega L_{s}}{2 \pi} I_{d} \\
& V_{d}=1.35 V_{L L} \cos \alpha-3 \frac{\omega L_{s}}{\pi} I_{d} \\
& \cos (\alpha+u)=\cos \alpha-2 \frac{\omega L_{S}}{\sqrt{2} V_{L L}} I_{d} \\
& \gamma=180-(\alpha+u)
\end{aligned}
$$

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$$
\begin{aligned}
& V_{L}=\left[\frac{1}{T} \int_{0}^{T} V_{L}^{2}(t) d t\right]^{1 / 2} \\
& V_{d c}=\frac{1}{T} \int_{0}^{T} v_{L}(t) d t \\
& \text { TUF }=\frac{P_{d c}}{V_{s} I_{s}}=\frac{V_{d k} I_{d k}}{V_{s} I_{s}} \\
& \quad \text { RF }=\frac{V_{a c}}{V_{d c}} \\
& \left(V_{\text {peak }}-V_{\min }\right)=\frac{2 P \Delta t}{\left(V_{\text {peak }}+V_{\min }\right) C}
\end{aligned}
$$

$$
\frac{d i_{L}}{d t}=\frac{V_{\text {in }}-V_{o u t}}{L}
$$

$$
\sigma=\frac{P_{d c}}{P_{L}}=\frac{V_{d c} T_{d c}}{V_{L} I_{L}}
$$

$$
\mathrm{FF}=\frac{V_{L}}{V_{d c}} \text { or } \frac{I_{L}}{I_{d c}}
$$

$$
V_{d \alpha}=\frac{1}{2 \pi} \int_{\alpha}^{\pi} V_{\max } \sin (\omega t) d(\omega t)=\frac{V_{\max }}{2 \pi}(1+\cos \alpha)
$$

$V_{p h}=\frac{V}{\sqrt{3}}, I_{p h}=I$ for star connection, $V_{p h}=V, I_{p h}=\frac{I}{\sqrt{3}}$ for delta connection
$S=\sqrt{3} V I \quad V . A, P=\sqrt{3} V I \cos \theta W ., Q=\sqrt{3} V I \sin \theta V . A \cdot r$
$Q_{C}=\sqrt{3} V I_{C}$ V.A.r, $X_{C}=\frac{V}{\sqrt{3} I_{C}} \Omega$

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Three-phase systems


Delta to Star conversion:


Star to Delta conversion:
Gravity:
interface material:

Output voltage of a differentiator circuit:

Compressibility relationship:

General manometer:

$$
R_{c}=\frac{R_{3} R_{1}}{R_{1}+R_{2}+R_{3}}
$$

$$
R_{1}=\frac{R_{a} R_{b}+R_{b} R_{c}+R_{c} R_{a}}{R_{b}}
$$

$$
R_{2}=\frac{R_{a} R_{b}+R_{b} R_{c}+R_{c} R_{a}}{R_{c}}
$$

$$
R_{3}=\frac{R_{a} R_{b}+R_{b} R_{c}+R_{c} R_{a}}{R_{a}}
$$

$$
9.81 \mathrm{~m} / \mathrm{s}
$$

$$
\theta_{c s}=\frac{(\rho)(t)}{A}
$$

$$
\begin{aligned}
& R_{a}=\frac{R_{1} R_{2}}{R_{1}+R_{2}+R_{3}} \\
& R_{b}=\frac{R_{2} R_{3}}{R_{1}+R_{2}+R_{3}}
\end{aligned}
$$

$$
v_{0}=-R_{2} C_{1} \frac{d v_{I}}{d t}
$$

$$
K=-V \frac{d P}{d V}
$$

$\Delta \mathrm{P}=|\Delta \rho \mathrm{g} \Delta \mathrm{h}|$

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Venturi meter:

$$
v_{\text {in }}=C_{D} \sqrt{\frac{2 \Delta P}{\rho_{f}\left[\left(\frac{d_{\text {large }}}{d_{\text {small }}}\right)^{4}-1\right]}}
$$

Force on a submerged wall:

$$
F=\frac{\rho g a h^{2}}{2}
$$

Drag coefficient:

$$
C_{D \text { rag }}=\frac{F_{D}}{\frac{1}{2} \rho v^{2} A}
$$

Flow through a small hole:

$$
Q=C_{D} \sqrt{\frac{2 \Delta P}{\rho}} A
$$

Flow through a rectangular slit:

$$
Q=\frac{2}{3} C_{D} W \sqrt{2 g}\left[(H o+L)^{\frac{3}{2}}-H o^{\frac{3}{2}}\right]
$$

Tank draining:

$$
h^{\frac{1}{2}}=h_{0}^{\frac{1}{2}}-\frac{C_{D} a \sqrt{2 g}}{2 A} t
$$

Flow over a rectangular weir:

$$
Q=\frac{2}{3} C_{D} W \sqrt{2 g} H^{\frac{3}{2}}
$$

Flow over a V-notch weir:

Poisseuille's Law:

$$
Q=\frac{8}{15} C_{D} \tan (\theta / 2)(2 g)^{\frac{1}{2}} H^{\frac{5}{2}}
$$

$$
Q=-\frac{\pi}{128 \mu} \frac{d P}{d x} D^{4}
$$

$$
\Delta P=\frac{2 f L \rho \bar{u}^{2}}{D}
$$

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Summary of phase and line voltages/currents for balanced three-phase systems. ${ }^{1}$
Connection Phase voltages/currents Line voltages/currents

| Y-Y | $\begin{aligned} & \mathbf{V}_{a n}=V_{p} / 0^{\circ} \\ & \mathbf{V}_{b n}=V_{p}\left\lfloor-120^{\circ}\right. \\ & \mathbf{V}_{c n}=V_{p} \angle+120^{\circ} \end{aligned}$ <br> Same as line currents | $\begin{aligned} & \mathbf{V}_{a b}=\sqrt{3} V_{p} / 30^{\circ} \\ & \mathbf{V}_{b c}=\mathbf{V}_{a b} /-120^{\circ} \\ & \mathbf{V}_{c a}=\mathbf{V}_{a b} /+120^{\circ} \\ & \mathbf{I}_{a}=\mathbf{V}_{a n} / \mathbf{Z}_{Y} \\ & \mathbf{I}_{b}=\mathbf{I}_{a} /-120^{\circ} \\ & \mathbf{I}_{c}=\mathbf{I}_{a} /+120^{\circ} \end{aligned}$ |
| :---: | :---: | :---: |
| Y- $\Delta$ | $\begin{aligned} & \mathbf{V}_{a n}=V_{p} / 0^{\circ} \\ & \mathbf{V}_{b n}=V_{p} /-120^{\circ} \\ & \mathbf{V}_{c n}=V_{p} /+120^{\circ} \\ & \mathbf{I}_{A B}=\mathbf{V}_{A B} / \mathbf{Z}_{\Delta} \\ & \mathbf{I}_{B C}=\mathbf{V}_{B C} / \mathbf{Z}_{\Delta} \\ & \mathbf{I}_{C A}=\mathbf{V}_{C A} / \mathbf{Z}_{\Delta} \end{aligned}$ | $\begin{aligned} & \mathbf{V}_{a b}=\mathbf{V}_{A B}=\sqrt{3} V_{p} \angle 30^{\circ} \\ & \mathbf{V}_{b c}=\mathbf{V}_{B C}=\mathbf{V}_{a b} /-120^{\circ} \\ & \mathbf{V}_{c a}=\mathbf{V}_{C A}=\mathbf{V}_{a b} \angle+120^{\circ} \\ & \mathbf{I}_{a}=\mathbf{I}_{A B} \sqrt{3} /-30^{\circ} \\ & \mathbf{I}_{b}=\mathbf{I}_{a} /-120^{\circ} \\ & \mathbf{I}_{c}=\mathbf{I}_{a} /+120^{\circ} \end{aligned}$ |
| $\Delta-\Delta$ | $\begin{aligned} & \mathbf{V}_{a b}=V_{p} / 0^{\circ} \\ & \mathbf{V}_{b c}=V_{p} /-120^{\circ} \\ & \mathbf{V}_{c a}=V_{p} /+120^{\circ} \\ & \mathbf{I}_{A B}=\mathbf{V}_{a b} / \mathbf{Z}_{\Delta} \\ & \mathbf{I}_{B C}=\mathbf{V}_{b c} / \mathbf{Z}_{\Delta} \\ & \mathbf{I}_{C A}=\mathbf{V}_{c a} / \mathbf{Z}_{\Delta} \end{aligned}$ | Same as phase voltages $\begin{aligned} & \mathbf{I}_{a}=\mathbf{I}_{A B} \sqrt{3} /-30^{\circ} \\ & \mathbf{I}_{b}=\mathbf{I}_{a} /-120^{\circ} \\ & \mathbf{I}_{c}=\mathbf{I}_{a} /+120^{\circ} \end{aligned}$ |
| $\Delta$-Y | $\begin{aligned} \mathbf{V}_{a b} & =V_{p} / 0^{\circ} \\ \mathbf{V}_{b c} & =V_{p} /-120^{\circ} \\ \mathbf{V}_{c a} & =V_{p} /+120^{\circ} \end{aligned}$ | Same as phase voltages |

Same as line currents

$$
\begin{aligned}
& \mathbf{I}_{a}=\frac{V_{p} L-30^{\circ}}{\sqrt{3} \mathbf{Z}_{Y}} \\
& \mathbf{I}_{b}=\mathbf{I}_{a} /-120^{\circ} \\
& \mathbf{I}_{c}=\mathbf{I}_{a} /+120^{\circ}
\end{aligned}
$$

